48VG-A and 48VG-B
Performance ${ }^{\text {ma }}$ 15-16 SEER 2-Stage Packaged Air
Conditioner and Gas Furnace System with Puron
(R-410A) Refrigerant
Single and Three Phase

2-5 Nominal Tons (Sizes 24-60)

## Installation Instructions

IMPORTANT: Effective January 1, 2015, all split system and packaged air conditioners must be installed pursuant to applicable regional efficiency standards issued by the Department of Energy.
NOTE: Read the entire instruction manual before starting the installation.
NOTE: Installer: Make sure the Owner's Manual and Service Instructions are left with the unit after installation.

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A09033
Fig. 1 - Unit 48VG (Low NOx Model Available)
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## SAFETY CONSIDERATIONS

Improper installation, adjustment, alteration, service maintenance, or use can cause explosion, fire, electrical shock, or other conditions which may cause death, personal injury, or property damage. Consult a qualified installer, service agency, or your distributor or branch for information or assistance. The qualified installer or agency must use factory-authorized kits or accessories when modifying this product. Refer to the individual instructions packaged with the kits or accessories when installing.
Follow all safety codes. Wear safety glasses, protective clothing, and work gloves. Have a fire extinguisher available. Read these instructions thoroughly and follow all warnings or cautions included in literature and attached to the unit. consult local building codes, the current editions of the National Fuel Gas Code (NFGC) NFPA 54/ANSI Z223.1, and the National Electrical Code (NEC) NFPA 70.
In Canada refer to the current editions of the National Standards of Canada CAN/CSA-B149.1 and . 2 Natural Gas and Propane Installation codes, and Canadian Electrical Code CSA C22.1

Recognize safety information. This is the safety-alert symbol $\triangle$. When you see this symbol on the unit and in instructions or manuals, be alert to the potential for personal injury. Understand these signal words: DANGER, WARNING, and CAUTION. These words are used with the safety-alert symbol. DANGER identifies the most serious hazards which will result in severe personal injury or death. WARNING signifies hazards which could result in personal injury or death. CAUTION is used to identify unsafe practices which may result in minor personal injury or product and property damage. NOTE is used to highlight suggestions which will result in enhanced installation, reliability, or operation.

## 4 WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.
Before installing or servicing system, always turn off main power to system and install lockout tag. There may be more than one disconnect switch. Turn off accessory heater power switch if applicable.

## 4 WARNING

## PERSONAL INJURY AND ENVIRONMENTAL HAZARD

Failure to relieve system pressure could result in personal injury and/or death.

1. Relieve pressure and recover all refrigerant before servicing existing equipment, and before final unit disposal. Use all service ports and open all flow-control devices, including solenoid valves.
2. Federal regulations require that you do not vent refrigerant into the atmosphere. Recover during system repair or final unit disposal.

## 4 WARNING

## FIRE, EXPLOSION, ELECTRICAL SHOCK AND CARBON MONOXIDE POISONING HAZARD

Failure to follow this warning could result in personal injury or unit damage.
A qualified installer or agency must use only factory-authorized kits or accessories when modifying this product.

## 4 CAUTION

## CUT HAZARD

Failure to follow this caution may result in personal injury. When removing access panels (see Fig. 17) or performing maintenance functions inside your unit, be aware of sharp sheet metal parts and screws. Although special care is taken to reduce sharp edges to a minimum, be extremely careful and wear appropriate protective clothing, safety glasses and gloves when handling parts or reaching into the unit.

## INTRODUCTION

This unit (see Fig. 1) is a fully self-contained, combination Category I gas heating/electric cooling unit designed for outdoor installation (See Fig. 3 and 6 for unit dimensions). All unit sizes have return and discharge openings for both horizontal and downflow configurations, and are factory shipped with all downflow duct openings covered. Units may be installed either on
a rooftop or on a cement slab. (See Fig. 7 for roof curb dimensions).
In gas heating mode, this unit is designed for a minimum continuous return-air temperature of $55^{\circ} \mathrm{F}\left(13^{\circ} \mathrm{C}\right) \mathrm{db}$ and a maximum continuous return-air temperature of $80^{\circ} \mathrm{F}\left(27^{\circ} \mathrm{C}\right) \mathrm{db}$. Failure to follow these return-air temperature limits may affect reliability of heat exchangers, motors, and other components.
Models with an N in the fifth position of the model number are dedicated Low NOx units designed for California installations. These models meet the California maximum oxides of nitrogen (NOx) emissions requirements of 40 nanograms/joule or less as shipped from the factory and must be installed in California Air Quality Management Districts or any other regions in North America where a Low NOx rule exists.
NOTE: Low NOx requirements apply only to natural gas installations.

## RECEIVING AND INSTALLATION

## Step 1 - Check Equipment

Identify Unit
The unit model number and serial number are stamped on the unit information plate. Check this information against shipping papers.

## Inspect Shipment

Inspect for shipping damage before removing packaging materials. If unit appears to be damaged or is torn loose from its anchorage, have it examined by transportation inspectors before removal. Forward claim papers directly to transportation company. Manufacturer is not responsible for any damage incurred in transit. Check all items against shipping list. Immediately notify the nearest equipment distribution office if any item is missing. To prevent loss or damage, leave all parts in original packages until installation.
If the unit is to be mounted on a curb in a downflow application, review Step 9 to determine which method is to be used to remove the downflow panels before rigging and lifting into place. The panel removal process may require the unit to be on the ground.

## Step 2 - Provide Unit Support

For hurricane tie downs, contact distributor for details and PE (Professional Engineering) Certificate if required.

## Roof Curb

Install accessory roof curb in accordance with instructions shipped with curb (See Fig. 7). Install insulation, cant strips, roofing, and flashing. Ductwork must be attached to curb.
IMPORTANT: The gasketing of the unit to the roof curb is critical for a water tight seal. Install gasketing material supplied with the roof curb. Improperly applied gasketing also can result in air leaks and poor unit performance.
Curb should be level to within $1 / 4 \mathrm{in}$. ( 6 mm ). This is necessary for unit drain to function properly. Refer to accessory roof curb installation instructions for additional information as required.

## Installation on older " $G$ " series roof curbs.

Two accessory kits are available to aid in installing a new "G" series unit on an old "G" roof curb.

1. Accessory kit number CPADCURB001A00, (small chassis) and accessory kit number CPADCURB002A00, (large chassis) includes roof curb adapter and gaskets for the perimeter seal and duct openings. No additional modifications to the curb are required when using this kit.
2. An alternative to the adapter curb is to modify the existing curb by removing the outer horizontal flange and use accessory kit number CPGSKTKIT001A00 which includes spacer blocks (for easy alignment to existing curb) and gaskets for the perimeter seal and duct openings. This kit is used when existing curb is modified by removing outer horizontal flange.

## UNITS/STRUCTURAL DAMAGE HAZARD

Failure to follow this caution may result in property damage.
Ensure there is sufficient clearance for saw blade when cutting the outer horizontal flange of the roof curb so there is no damage to the roof or flashing.

## Slab Mount

Place the unit on a solid, level pad that is at least 2 in . $(51 \mathrm{~mm})$ above grade. The pad should extend approximately 2 in . ( 51 mm ) beyond the casing on all 4 sides of the unit. (See Fig. 2.) Do not secure the unit to the pad except when required by local codes.


A07926
Fig. 2 - Slab Mounting Details

## Step 3 - Field Fabricate Ductwork

Secure all ducts to roof curb and building structure on vertical discharge units. Do not connect ductwork to unit. For horizontal applications, unit is provided with flanges on the horizontal openings. All ductwork should be secured to the flanges. Insulate and weatherproof all external ductwork, joints, and roof openings with counter flashing and mastic in accordance with applicable codes.
Ducts passing through an unconditioned space must be insulated and covered with a vapor barrier.
If a plenum return is used on a vertical unit, the return should be ducted through the roof deck to comply with applicable fire codes. Read unit rating plate for any required clearances around ductwork. Cabinet return-air static shall not exceed -. 25 IN. W.C.

## Step 4 - Provide Clearances

IMPORTANT: The unit must be secured to the curb by installing screws through the bottom of the curb flange and into the unit base rails. When installing large base units onto the common curb, the screws must be installed before allowing the full weight of the unit to rest on the curb. A minimum of six screws are required for large base units. Failure to secure unit properly could result in an unstable unit. See Warning near Rigging/Lifting information and accessory curb instructions for more details.
The required minimum operating and service clearances are shown in Fig. 3 and 6. Adequate combustion, ventilation and condenser air must be provided.
IMPORTANT: Do not restrict outdoor airflow. An air restriction at either the outdoor-air inlet or the fan discharge may be detrimental to compressor life.
The outdoor fan pulls air through the outdoor coil and discharges it through the top grille. Be sure that the fan discharge does not recirculate to the outdoor coil. Do not locate the unit in either a corner or under an overhead obstruction. The minimum clearance under a partial overhang (such as a normal house overhang) is 48 -in. ( 1219 mm ) above the unit top. The maximum horizontal extension of a partial overhang must not exceed $48-\mathrm{in}$. ( 1219 mm ).

Do not place the unit where water, ice, or snow from an overhang or roof will damage or flood the unit. Do not install the unit on carpeting or other combustible materials. Slab-mounted units should be at least 2 in . ( 51 mm ) above the highest expected water and runoff levels. Do not use unit if it has been under water.

## Step 5 - Rig and Place Unit

Rigging and handling of this equipment can be hazardous for many reasons due to the installation location (roofs, elevated structures, etc.).
Only trained, qualified crane operators and ground support staff should handle and install this equipment.
When working with this equipment, observe precautions in the literature, on tags, stickers, and labels attached to the equipment, and any other safety precautions that might apply.
Training for operators of the lifting equipment should include, but not be limited to, the following:

1. Application of the lifter to the load, and adjustment of the lifts to adapt to various sizes or kinds of loads.
2. Instruction in any special operation or precaution.
3. Condition of the load as it relates to operation of the lifting kit, such as balance, temperature, etc.
Follow all applicable safety codes. Wear safety shoes and work gloves.

## Inspection

Prior to initial use, and at monthly intervals, all rigging shackles, clevis pins, and straps should be visually inspected for any damage, evidence of wear, structural deformation, or cracks. Particular attention should be paid to excessive wear at hoist hooking points and load support areas. Materials showing any kind of wear in these areas must not be used and should be discarded.


## UNIT FALLING HAZARD

Failure to follow this warning could result in personal injury or death.
Never stand beneath rigged units or lift over people.

## WARNING

## PROPERTY DAMAGE HAZARD

Failure to follow this warning could result in personal injury/death or property damage.
When straps are taut, the clevis should be a minimum of 36 in. ( 914 mm ) above the unit top cover.

## Rigging/Lifting of Unit (See Fig. 8)

## 4 WARNING

## UNIT FALLING HAZARD

Failure to follow this warning could result in personal injury or death.
Large base units must be secured to common curb before allowing full weight of unit to rest on curb. Install screws through curb into unit base rails while rigging crane is still supporting unit.

Lifting holes are provided in base rails as shown in Fig. 3 and 6.

1. Leave top shipping skid on the unit for use as a spreader bar to prevent the rigging straps from damaging the unit. If the skid is not available, use a spreader bar of sufficient length to protect the unit from damage. mert
2. Attach shackles, clevis pins, and straps to the base rails of the unit. Be sure materials are rated to hold the weight of the unit (See Fig. 8).
3. Attach a clevis of sufficient strength in the middle of the straps. Adjust the clevis location to ensure unit is lifted level with the ground.

After the unit is placed on the roof curb or mounting pad, remove the top skid.


Fig. 3-48VG-A30 Unit Dimensions


Fig. 4 - 48VG-B24-30 Unit Dimensions


A14628
Fig. 5-48VG-A36-60 Unit Dimensions

| UNIT | ELECTRICAL CHARACTERISTICS | UNIT WT. |  | UNIT HEIGHT IN/MM |  | CENTER OF GRAVITY IN/MM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LB | KG | "A" |  | X |  | Y |  | Z |  |
| 48VG(-/N)B36(060/090)30(--/GP/GS/TF/TP) | 208/230-1-60 | 447 | 202.8 | 44-3/4 | 1137 | 22-13/16 | 579.4 | 18 | 457.2 | 17-1/8 | 435.0 |
| 48VG(-/N)B42(060/090)30(--/GP/GS/TF/TP) | 208/230-1-60 | 447 | 202.8 | 44-3/4 | 1137 | 22-13/16 | 579.4 | 18 | 457.2 | 17-1/8 | 435.0 |
| $48 \mathrm{VG}(-/ \mathrm{N})$ B48(090/115/130)30(--/GP/GS/TF/TP) | 208/230-1.60 | 492 | 223.2 | 50-3/4 | 1289 | 22-13/16 | 579.4 | 18 | 457.2 | 17-3/8 | 441.3 |
| $48 \mathrm{VG}(-/ \mathrm{N}) \mathrm{B60}(090 / 115 / 130) 30(--/ G P / G S /$ TF/TP $)$ | 208/230-1-60 | 512 | 232.2 | 52-3/4 | 1340 | 22-13/16 | 579.4 | 18 | 457.2 | 17-5/8 | 447.7 |
| 48VG(-/N)A36(060/090)(5/6)0(--/GS/TF) | 208/230-3-60,460-3 | 447 | 202.8 | 44-3/4 | 1137 | 22-13/16 | 579.4 | 18 | 457.2 | 17-1/8 | 435.0 |
| 48VG( -/N)A42 (060/090)(5/6)0(--/GS/TF) | 208/230-3-60,460-3 | 447 | 202.8 | 44-3/4 | 1137 | 22-13/16 | 579.4 | 18 | 457.2 | 17-1/8 | 435.0 |
| $48 \mathrm{VG}(-/ \mathrm{N})$ A $48(090 / 115 / 130)(5 / 6) 0(\cdots / G S /$ IF $)$ | 208/230-3-60,460-3 | 492 | 223.2 | 50-3/4 | 1289 | 22-13/16 | 579.4 | 18 | 457.2 | 17-3/8 | 441.3 |
| $48 \mathrm{VG}(-/ \mathrm{N})$ A60 (090/115/130)(5/6)0( - /GS/TF) | 208/230-3-60,460-3 | 512 | 232.2 | 52-3/4 | 1340 | 22-13/16 | 579.4 | 18 | 457.2 | 17-5/8 | 447.7 |


 dimensions in [] are in mm


A150033
Fig. 6-48VG-B36-60 Unit Dimensions



LARGE CURB

A09415


UNIT PLACEMENT ON COMMON CURB

SMALL OR LARGE BASE UNIT

| $\begin{aligned} & \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | CATALOG NUMBER | $\begin{gathered} \text { A } \\ \text { IN. } \\ (\mathrm{mm}) \end{gathered}$ | B (small / common base) IN. (mm)* | $\begin{gathered} \text { B (large } \\ \text { base) } \\ \text { IN. (mm)* } \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { IN. } \\ (\mathrm{mm}) \end{gathered}$ |  | $E$ IN. $(\mathrm{mm})$ | $\underset{(\mathrm{Fm})}{\mathrm{F} .}$ | $\stackrel{\mathrm{G}}{\mathrm{IN} .(\mathrm{mm})}$ | IN. (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Small } \\ & \text { or } \\ & \text { Large } \end{aligned}$ | CPRFCURB010A00 | $\begin{gathered} 11 \\ (279) \end{gathered}$ | 10 (254) | 14 (356) | $\begin{gathered} 16 \\ (406) \end{gathered}$ | $\begin{gathered} 47.8 \\ (1214) \end{gathered}$ | $\begin{gathered} 32.4 \\ (822) \end{gathered}$ | 2.7 (69) | 30.6 (778) | 46.1 (1170) |
|  | CPRFCURB011A00 | $\begin{gathered} 14 \\ (356) \end{gathered}$ |  |  |  |  |  |  |  |  |
| Large | CPRFCURB012A00 | $\begin{gathered} 11 \\ (279) \end{gathered}$ | 14 (356) |  |  |  | $\begin{gathered} 43.9 \\ (1116) \end{gathered}$ |  | 42.2 (1072) |  |
|  | CPRFCURB013A00 | $\begin{gathered} 14 \\ (356) \end{gathered}$ |  |  |  |  |  |  |  |  |

[^0]Fig. 7 - Roof Curb Dimensions

## ^ CAUTION - NOTICE TO RIGGERS <br> A PRUDENCE - AVIS AUX MANIPULATEUR

ACCESS PANELS MUST BE IN PLACE WHEN RIGGING.
PANNEAUX D'ACCES DOIT ÊTRE EN PLACE POUR MANIPULATION.
Use top skid as spreader bar. / Utiliser la palette du haut comme barre de répartition


Standard Copper Tube Aluminum Fin

| SMALL CABINET |  |  |  |  | LARGE CABINET |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24 |  | 30 |  | Unit | 36 |  | 42 |  | 48 |  | 60 |  |
| Unit | lb | kg | lb | kg |  | lb | kg | lb | kg | lb | kg | lb | kg |
| Rigging Weight | 352 | 160 | 359 | 163 | Rigging Weight | 455 | 206 | 455 | 206 | 500 | 227 | 520 | 236 |

NOTE: See dimensional drawing for corner weights.
Optional Copper Tube Copper Fin

| SMALL CABINET |  |  |  |  | LARGE CABINET |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unit | 24 |  | 30 |  | Unit | 36 |  | 42 |  | 48 |  | 60 |  |
|  | lb | kg | lb | kg |  | lb | kg | lb | kg | lb | kg | lb | kg |
| Rigging Weight | 390 | 177 | 416 | 189 | Rigging Weight | 517 | 235 | 517 | 235 | 584 | 265 | 610 | 277 |

NOTE: See dimensional drawing for corner weights.
Fig. 8 - Suggested Rigging

Table 1 - Physical Data

*Based on altitude of 0 to 2000 ft ( $0-610 \mathrm{~m}$ ).
$\dagger$ Required filter sizes shown are based on the larger of the AHRI (Air Conditioning Heating and Refrigeration Institute) rated cooling airflow or the heating airflow velocity of $300 \mathrm{ft} / \mathrm{minute}$ for throwaway type. Air filter pressure drop for non-standard filters must not exceed 0.08 IN. W.C.
$\ddagger$ If using accessory filter rack refer to the filter rack installation instructions for correct filter sizes and quantity.

Table 1—Physical Data Con't

| UNIT SIZE | 48090 | 48115 | 48130 | 60090 | 60115 | 60130 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NOMINAL CAPACITY (ton) | 4 | 4 | 4 | 5 | 5 | 5 |
| SHIPPING WEIGHT lb SHIPPING WEIGHT kg | $\begin{aligned} & 500 \\ & 227 \end{aligned}$ | $\begin{aligned} & 500 \\ & 227 \end{aligned}$ | $\begin{aligned} & 500 \\ & 227 \end{aligned}$ | $\begin{aligned} & 520 \\ & 236 \end{aligned}$ | $\begin{aligned} & 520 \\ & 236 \end{aligned}$ | $\begin{aligned} & 520 \\ & 236 \end{aligned}$ |
| COMPRESSORS | Scroll |  |  |  |  |  |
| Quantity | 1 |  |  |  |  |  |
| REFRIGERANT (R-410A) <br> Quantity lb <br> Quantity (kg.) | $\begin{gathered} 10.8 \\ 4.9 \end{gathered}$ | $\begin{gathered} 10.8 \\ 4.9 \end{gathered}$ | $\begin{gathered} 10.8 \\ 4.9 \end{gathered}$ | $\begin{gathered} 12.1 \\ 5.5 \end{gathered}$ | $\begin{gathered} 12.1 \\ 5.5 \end{gathered}$ | $\begin{gathered} 12.1 \\ 5.5 \end{gathered}$ |
| REFRIGERANT METERING DEVICE | TXV |  |  |  |  |  |
| OUTDOOR COIL <br> Rows...Fins/in. Face Area (sq ft) | $\begin{gathered} 2 \ldots . .21 \\ 19.4 \end{gathered}$ | $\begin{gathered} 2 . . .21 \\ 19.4 \end{gathered}$ | $\begin{gathered} 2 \ldots . .21 \\ 19.4 \end{gathered}$ | $\begin{gathered} 2 . . .21 \\ 21.4 \end{gathered}$ | $\begin{gathered} 2 . . .21 \\ 21.4 \end{gathered}$ | $\begin{gathered} 2 \ldots . .21 \\ 21.4 \end{gathered}$ |
| OUTDOOR FAN <br> Nominal Cfm Diameter in. Diameter (mm) Motor Hp (Rpm) | $\begin{gathered} 3300 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ | $\begin{gathered} 3300 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ | $\begin{gathered} 3300 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ | $\begin{gathered} 3600 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ | $\begin{gathered} 3600 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ | $\begin{gathered} 3600 \\ 26 \\ 660.4 \\ 1 / 5(810) \end{gathered}$ |
| INDOOR COIL Rows...Fins/in. Face Area (sq ft) | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ | $\begin{gathered} 3 . .17 \\ 5.7 \end{gathered}$ |
| INDOOR BLOWER <br> Nominal Low Stage Cooling Airflow (Cfm) Nominal High Stage Cooling Airflow (Cfm) Size in. <br> Size (mm) <br> Motor HP (RPM) | $\begin{gathered} 1200 \\ 1600 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \\ \hline \end{gathered}$ | $\begin{gathered} 1200 \\ 1600 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \end{gathered}$ | $\begin{gathered} 1200 \\ 1600 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \end{gathered}$ | $\begin{gathered} 1200 \\ 1750 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \end{gathered}$ | $\begin{gathered} 1200 \\ 1750 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \end{gathered}$ | $\begin{gathered} 1200 \\ 1750 \\ 11 \times 10 \\ 279.4 \times 254 \\ 1.0(1075) \\ \hline \end{gathered}$ |
| FURNACE SECTION* <br> Burner Orifice No. (Qty...Drill Size) <br> Natural Gas (Factory Installed) <br> Propane Gas | $\begin{aligned} & 3 . . .38 \\ & 3 . . .53 \end{aligned}$ | $\begin{aligned} & 3 . . .33 \\ & 3 . . .51 \end{aligned}$ | $\begin{aligned} & 3 . . .31 \\ & 3 . . .49 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3 . . .38 \\ & 3 . . .53 \end{aligned}$ | $\begin{aligned} & 3 . . .33 \\ & 3 . . .51 \end{aligned}$ | $\begin{aligned} & 3 . . .31 \\ & 3 . .49 \\ & \hline \end{aligned}$ |
| HIGH-PRESSURE SWITCH (psig) Cut-out Reset (Auto) | $\begin{aligned} & 650+/-15 \\ & 420+/-25 \end{aligned}$ |  |  |  |  |  |
| LOSS-OF-CHARGE / LOW-PRESSURE SWITCH (psig) cut-out Reset (auto) | $\begin{gathered} 50+/-7 \\ 95+/-7 \end{gathered}$ |  |  |  |  |  |
| RETURN-AIR FILTERS Throwaway $\ddagger \ddagger$ in. (mm) | $\begin{gathered} 24 \times 36 \times 1 \\ 610 \times 914 \times 25 \end{gathered}$ |  |  |  |  |  |
| *Based on altitude of 0 to 2000 ft (0-610 m). <br> $\dagger$ Required filter sizes shown are based on the larger of the AHRI (Air Conditioning Heating and Refrigeration Institute) rated cooling airflow or the heating airflow velocity of $300 \mathrm{ft} /$ minute for throwaway type. Air filter pressure drop for non-standard filters must not exceed 0.08 IN. W.C. <br> $\ddagger$ If using accessory filter rack refer to the filter rack installation instructions for correct filter sizes and quantity. |  |  |  |  |  |  |

## Step 6 - Connect Condensate Drain

NOTE: When installing condensate drain connection be sure to comply with local codes and restrictions.
Model $48 \mathrm{VG}-\mathrm{A}$ disposes of condensate water through a $3 / 4 \mathrm{in}$. NPT fitting which exits through the base on the evaporator coil access side. See Fig. 3 \& 6 for location.
Condensate water can be drained directly onto the roof in rooftop installations (where permitted) or onto a gravel apron in ground level installations. Install a field-supplied 2-in. ( 51 mm ) condensate trap at the end of condensate connection to ensure proper drainage. Make sure that the outlet of the trap is at least 1 in . $(25 \mathrm{~mm})$ lower than the drain-pan condensate connection to prevent the pan from overflowing (See Fig. 9). Prime the trap with water. When using a gravel apron, make sure it slopes away from the unit.


Fig. 9 - Condensate Trap
Connect a drain tube using a minimum of $3 / 4-\mathrm{in}$. PVC or $3 / 4-\mathrm{in}$. copper pipe (all field-supplied) at the outlet end of the $2-\mathrm{in}$. ( 51 mm ) trap. Do not undersize the tube. Pitch the drain tube downward at a slope of at least 1-in. ( 25 mm ) for every 10 ft (3.1 $\mathrm{m})$ of horizontal run. Be sure to check the drain tube for leaks.

## Step 7 — Install Flue Hood

The flue assembly is secured and shipped in the return air duct. Remove duct cover to locate the assembly (See Fig. 11).
NOTE: Dedicated low NOx models MUST be installed in California Air Quality Management Districts where a Low NOx rule exists.

These models meet the California maximum oxides of nitrogen (NOx) emissions requirements of 40 nanograms/joule or less as shipped from the factory.
NOTE: Low NOx requirements apply only to natural gas installations.

## WARNING

## CARBON MONOXIDE POISONING HAZARD

Failure to follow this warning could result in personal injury or death.
The venting system is designed to ensure proper venting. The flue hood assembly must be installed as indicted in this section of the unit installation instructions.

Install the flue hood as follows:

1. This installation must conform with local building codes and with NFPA 54/ANSI Z223.1 National Fuel Gas Code (NFGC), (in Canada, CAN/CGA B149.1, and B149.2) latest revision. Refer to Provincial and local plumbing or wastewater codes and other applicable local codes.
2. Remove flue hood from shipping location (inside the return section of the blower compartment-see Fig. 11). Remove the return duct cover to locate the flue hood. Place flue
hood assembly over flue panel. Orient screw holes in flue hood with holes in the flue panel.
3. Secure flue hood to flue panel by inserting a single screw on the top flange and the bottom flange of the hood.

## Step 8 - Install Gas Piping

The gas supply pipe enters the unit through the access hole provided. The gas connection to the unit is made to the $1 / 2-\mathrm{in}$. $(12.7 \mathrm{~mm})$ FPT gas inlet on the gas valve.
Install a gas supply line that runs to the heating section. Refer to the NFGC for gas pipe sizing. Do not use cast-iron pipe. It is recommended that a black iron pipe is used. Check the local utility for recommendations concerning existing lines. Size gas supply piping for 0.5 IN . W.C. maximum pressure drop. Never use pipe smaller than the $1 / 2-\mathrm{in}$. $(12.7 \mathrm{~mm})$ FPT gas inlet on the unit gas valve.
For natural gas applications, the gas pressure at unit gas connection must not be less than 4.0 IN . W.C. or greater than 13 IN . W.C. while the unit is operating. For propane applications, the gas pressure must not be less than 11.0 IN . W.C. or greater than 13 IN . W.C. at the unit connection.

A $1 / 8-\mathrm{in}$. ( 3.2 mm ) NPT plugged tapping, accessible for test gauge connection, must be installed immediately upstream of the gas supply connection to the gas valve.
When installing the gas supply line, observe local codes pertaining to gas pipe installations. Refer to the NFPA 54/ANSI Z223.1 latest edition (in Canada, CAN/CGA B149.1).
NOTE: In the state of Massachusetts:

1. Gas supply connections MUST be performed by a licensed plumber or gas fitter.
2. When flexible connectors are used, the maximum length shall not exceed 36 inches ( 915 mm ).
3. When lever handle type manual equipment shutoff valves are used, they shall be T-handle valves.
4. The use of copper tubing for gas piping is NOT approved by the state of Massachusetts.
In the absence of local building codes, adhere to the following pertinent recommendations:
5. Avoid low spots in long runs of pipe. Grade all pipe $1 / 4 \mathrm{in}$. $(6.35 \mathrm{~mm})$ for every $15 \mathrm{ft}(4.6 \mathrm{~m})$ of length to prevent traps. Grade all horizontal runs downward to risers. Use risers to connect to heating section and to meter.
6. Protect all segments of piping system against physical and thermal damage. Support all piping with appropriate straps,
hangers, etc. Use a minimum of one hanger every $6 \mathrm{ft}(1.8$ m ). For pipe sizes larger than $1 / 2$ in., follow recommendations of national codes.
7. Apply joint compound (pipe dope) sparingly and only to male threads of joint when making pipe connections. Use only pipe dope that is resistant to action of liquefied petroleum gases as specified by local and/or national codes. Never use Teflon tape.
8. Install sediment trap in riser leading to heating section (See Fig. 10). This drip leg functions as a trap for dirt and condensate.
9. Install an accessible, external, manual main shutoff valve in gas supply pipe within $6 \mathrm{ft}(1.8 \mathrm{~m})$ of heating section.
10. Install ground-joint union close to heating section between unit manual shutoff and external manual main shut-off valve.
11. Pressure test all gas piping in accordance with local and national plumbing and gas codes before connecting piping to unit.


C99020
Fig. 10 - Sediment Trap
NOTE: Pressure test the gas supply system after the gas supply piping is connected to the gas valve. The supply piping must be disconnected from the gas valve during the testing of the piping systems when test pressure is in excess of 0.5 psig . Pressure test the gas supply piping system at pressures equal to or less than 0.5 psig . The unit heating section must be isolated from the gas piping system by closing the external main manual shutoff valve and slightly opening the ground-joint union.

Table 2 - Maximum Gas Flow Capacity*

| NOMINAL IRON PIPE SIZE (IN.) | INTERNAL DIAMETER (IN.) | LENGTH OF PIPE FT (m) $\dagger$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \mathbf{1 0} \\ & (3) \\ & \hline \end{aligned}$ | $\begin{aligned} & 20 \\ & (6) \end{aligned}$ | $\begin{aligned} & 30 \\ & \text { (9) } \end{aligned}$ | $\begin{gathered} \hline 40 \\ (12) \end{gathered}$ | $\begin{gathered} 50 \\ (15) \end{gathered}$ | $\begin{gathered} 60 \\ (18) \end{gathered}$ | $\begin{gathered} 70 \\ \text { (21) } \end{gathered}$ | $\begin{gathered} 80 \\ (24) \end{gathered}$ | $\begin{gathered} 90 \\ (27) \end{gathered}$ | $\begin{aligned} & 100 \\ & (30) \end{aligned}$ | $\begin{aligned} & 125 \\ & (38) \end{aligned}$ | $\begin{aligned} & 150 \\ & (46) \end{aligned}$ | $\begin{aligned} & 175 \\ & \text { (53) } \end{aligned}$ | $\begin{aligned} & 200 \\ & (61) \end{aligned}$ |
| 1/2 | . 622 | 175 | 120 | 97 | 82 | 73 | 66 | 61 | 57 | 53 | 50 | 44 | 40 | - | - |
| 3/4 | . 824 | 360 | 250 | 200 | 170 | 151 | 138 | 125 | 118 | 110 | 103 | 93 | 84 | 77 | 72 |
| 1 | 1.049 | 680 | 465 | 375 | 320 | 285 | 260 | 240 | 220 | 205 | 195 | 175 | 160 | 145 | 135 |
| 1-1/4 | 1.380 | 1400 | 950 | 770 | 600 | 580 | 530 | 490 | 460 | 430 | 400 | 360 | 325 | 300 | 280 |
| 1-1/2 | 1.610 | 2100 | 1460 | 1180 | 990 | 900 | 810 | 750 | 690 | 650 | 620 | 550 | 500 | 460 | 430 |

*Capacity of pipe in cu ft of gas per hr for gas pressure of 0.5 psig or less. Pressure drop of $0.5-\mathrm{IN}$. W.C. (based on a 0.60 specific gravity gas). Refer to Table 2 and National Fuel Gas Code NFPA 54/ANSI Z223.1.
$\dagger$ This length includes an ordinary number of fittings.

## 4 WARNING

## FIRE OR EXPLOSION HAZARD

Failure to follow this warning could result in personal injury, death and/or property damage.
-Connect gas pipe to unit using a backup wrench to avoid damaging gas controls.
-Never purge a gas line into a combustion chamber. Never test for gas leaks with an open flame. Use a commercially available soap solution made specifically for the detection of leaks to check all connections. A fire or explosion may result causing property damage, personal injury or loss of life.
-Use proper length of pipe to avoid stress on gas control manifold.
-If a flexible connector is required or allowed by authority having jurisdiction, black iron pipe shall be installed at furnace gas valve and extend a minimum of 2 in . ( 51 mm ) outside furnace casing.
-If codes allow a flexible connector, always use a new connector. Do not use a connector which has previously serviced another gas appliance.
8. Check for gas leaks at the field-installed and factory-installed gas lines after all piping connections have been completed. Use a commercially available soap solution (or method specified by local codes and/or regulations).

## Step 9 - Install Duct Connections

The unit has duct flanges on the supply- and return-air openings on the side and bottom of the unit. For downshot applications, the ductwork connects to the roof curb (See Fig. 3 and 6 for connection sizes and locations).

## Configuring Units for Downflow (Vertical) Discharge

## WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.
Before installing or servicing system, always turn off main power to system and install lockout tag. There may be more than one disconnect switch.

1. Open all electrical disconnects before starting any service work.
2. Remove horizontal (metal) duct covers to access vertical (downflow) discharge duct knockouts in unit basepan. (See Fig. 11.)

## A CAUTION

## PROPERTY DAMAGE HAZARD

Failure to follow this caution may result in property damage.
Collect ALL screws that were removed. Do not leave screws on rooftop as permanent damage to the roof may occur.
3. For single-phase models only, on the discharge side only, remove the insulation covering the downshot (plastic) knockout. Insulation is held in place with aluminum tape. Please note that large chassis units have 2 pieces of insula-
tion, and only the piece over the downshot knockout needs to be removed. Discard insulation.
4. To remove the downshot (plastic) knockouts for both supply and returns, break front and right side connecting tabs with a screwdriver and hammer. Push cover down to break rear and left side tabs. These plastic knockouts are held in place with tabs similar to an electrical knockout. Discard plastic knockout covers.
5. Set unit on roof curb.
6. Verify that the downshot ducts are aligned with the downshot knockout areas.
7. Re-install horizontal (metal) covers as needed to seal unit. Ensure opensings are air and watertight.
NOTE: The design and installation of the duct system must be in accordance with the standards of the NFPA for installation of nonresidence-type air conditioning and ventilating systems, NFPA 90A or residence-type, NFPA 90B; and/or local codes and ordinances.
Adhere to the following criteria when selecting, sizing, and installing the duct system:

1. Units are shipped for horizontal duct installation (by removing duct covers).
2. Select and size ductwork, supply-air registers, and return-air grilles according to American Society of Heating, Refrigeration and Air Conditioning Engineers (ASHRAE) recommendations.
3. Use flexible transition between rigid ductwork and unit to prevent transmission of vibration. The transition may be screwed or bolted to duct flanges. Use suitable gaskets to ensure weather tight and airtight seal.
4. All units must have field-supplied filters or accessory filter rack installed in the return-air side of the unit. Recommended sizes for filters are shown in Table 1.


Fig. 11 - Supply and Return Duct Opening
5. Size all ductwork for maximum required airflow (either heating or cooling) for unit being installed. Avoid abrupt duct size increases or decreases or performance may be affected.
6. Adequately insulate and weatherproof all ductwork located outdoors. Insulate ducts passing through unconditioned space, and use vapor barrier in accordance with latest issue of Sheet Metal and Air Conditioning Contractors National Association (SMACNA) and Air Conditioning Contractors of America (ACCA) minimum installation standards for heating and air conditioning systems. Secure all ducts to building structure.
7. Flash, weatherproof, and vibration isolate all openings in building structure in accordance with local codes and good building practices.

## Step 10 - Install Electrical Connections

## 4 WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.

The unit cabinet must have an uninterrupted, unbroken electrical ground. This ground may consist of an electrical wire connected to the unit ground screw in the control compartment, or conduit approved for electrical ground when installed in accordance with NFPA 70 (NEC) (latest edition) (in Canada, Canadian Electrical Code CSA C22.1) and local electrical codes.

## CAUTION

## UNIT COMPONENT DAMAGE HAZARD

Failure to follow this caution may result in damage to the unit being installed.

1. Make all electrical connections in accordance with NFPA 70 (NEC) (latest edition) and local electrical codes governing such wiring. In Canada, all electrical connections must be in accordance with CSA standard C22.1 Canadian Electrical Code Part 1 and applicable local codes. Refer to unit wiring diagram.
2. Use only copper conductor for connections between field-supplied electrical disconnect switch and unit. DO NOT USE ALUMINUM WIRE.
3. Be sure that high-voltage power to unit is within operating voltage range indicated on unit rating plate. On 3 -phase units, ensure phases are balanced within 2 percent. Consult local power company for correction of improper voltage and/or phase imbalance.
4. Insulate low-voltage wires for highest voltage contained within conduit when low-voltage control wires are in same conduit as high-voltage wires.
5. Do not damage internal components when drilling through any panel to mount electrical hardware, conduit, etc.

## High-Voltage Connections

When routing power leads into unit, use only copper wire between disconnect and unit. The high voltage leads should be in a conduit until they enter the duct panel; conduit termination at the duct panel must be watertight.
The unit must have a separate electrical service with a field-supplied, waterproof disconnect switch mounted at, or within sight from, the unit. Refer to the unit rating plate, NEC and local
codes for maximum fuse/circuit breaker size and minimum circuit amps (ampacity) for wire sizing.
The field-supplied disconnect switch box may be mounted on the unit over the high-voltage inlet hole when the standard power and low-voltage entry points are used (See Fig. 3 and 4 for acceptable location).
NOTE: Field supplied disconnect switch box should be positioned so that it does not cover up any of the unit gas combustion supply air louvers.
See unit wiring label (Fig. 17, 18 and 19) and Fig. 12 for reference when making high voltage connections. Proceed as follows to complete the high-voltage connections to the unit.
Single phase units:

1. Run the high-voltage (L1, L2) and ground lead into the control box.
2. Connect ground lead to chassis ground connection.
3. Locate the black and yellow wires connected to the line side of the contactor (if equipped).
4. Connect field L1 to black wire from connection 11 of the compressor contactor.
5. Connect field wire L2 to yellow wire from connection 23 of the compressor contactor.
Three-phase units:
6. Run the high-voltage (L1, L2, L3) and ground lead into the control box.
7. Connect ground lead to chassis ground connection.
8. Locate the black and yellow wires connected to the line side of the contactor (if equipped).
9. Connect field L1 to black wire from connection 11 of the compressor contactor.
10. Connect field wire L3 to yellow wire from connection 13 of the compressor contactor.
11. Connect field wire L2 to blue wire from compressor.

## Special Procedures for 208-v Operation

## WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.
Make sure the power supply to the unit is switched OFF and install lockout tag. before making any wiring changes. With disconnect switch open, move black wire from transformer ( $3 / 16 \mathrm{in}$. 4.8 mm ]) terminal marked 230 to terminal marked 208. This retaps transformer to primary voltage of 208 vac .

## 1 WARNING

## ELECTRICAL SHOCK FIRE/EXPLOSION HAZARD

Failure to follow this warning could result in personal injury or death and property damage.
Before making any wiring changes, make sure the gas supply is switched off first. Then switch off the power supply to the unit and install lockout tag.

## Control Voltage Connections

Do not use any type of power-stealing thermostat. Unit control problems may result.
Use no. 18 American Wire Gage (AWG) color-coded, insulated ( $35^{\circ} \mathrm{C}$ minimum) wires to make the control voltage connections between the thermostat and the unit. If the thermostat is located more than $100 \mathrm{ft}(30.5 \mathrm{~m})$ from the unit (as measured along the control voltage wires), use no. 16 AWG color-coded, insulated ( $35^{\circ} \mathrm{C}$ minimum) wires.

## Standard Connection

Run the low-voltage leads from the thermostat, through the inlet hole, and into unit low-voltage splice box.
Locate eight (six for 460V 3-phase) 18-gage wires leaving control box. These low-voltage connection leads can be identified by the colors red, green, yellow, brown, blue, and white (See Fig. 12). Ensure the leads are long enough to be routed into the low-voltage splice box (located below right side of control box). Route leads through hole in bottom of control box and make low-voltage connections (See Fig. 12). Secure all cut wires, so that they do not interfere with operation of unit.

Fig. 12 - High- and Control-Voltage Connections
IMPORTANT: Dehumidification control must open control circuit on humidity rise above set point.
Use of the dehumidification cooling fan speed requires use of either a 24 VAC dehumidistat or a thermostat which includes control of a 24 VAC dehumidistat connection. In either case, the dehumidification control must open the control circuit on humidity rise above the dehumidification set point.

## Heat Anticipator Setting (Electro-Mechanical Thermostats only)

The room thermostat heat anticipator must be properly adjusted to ensure proper heating performance. Set the heat anticipator, using an ammeter between the W1 and R terminals to determine the exact required setting.
NOTE: For thermostat selection purposes, use 0.18 amp for the approximate required setting. Failure to make a proper heat anticipator adjustment will result in improper operation, discomfort to the occupants of the conditioned space, and inefficient energy utilization; however, the required setting may be changed slightly to provide a greater degree of comfort for a particular installation.

## Transformer Protection

The transformer is of the energy-limiting type, however a direct short will likely blow a secondary fuse. If an overload or short is present, correct overload condition and check for blown fuse on Indoor Fan board or Integrated Gas Controller. Replace fuse as required with correct size and rating.

## PRE-START-UP

1 WARNING

## ENVIRONMENTAL, FIRE, EXPLOSION, ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.

1. Follow recognized safety practices and wear protective goggles when checking or servicing refrigerant system.
2. Do not operate compressor or provide any electric power to unit unless compressor plug is in place and secured.
3. Do not remove compressor plug until all electrical sources are disconnected and tagged.
4. Relieve and recover all refrigerant from system before touching or disturbing compressor plug if refrigerant leak is suspected around compressor terminals.
5. Never attempt to repair soldered connection while refrigerant system is under pressure.
6. Do not use torch to remove any component. System contains oil and refrigerant under pressure.
To remove a component, wear protective goggles and proceed as follows:
a. Shut off electrical power to unit and install lockout tag.
b. Relieve and reclaim all refrigerant from system using both high- and low-pressure ports.
c. Cut component connecting tubing with tubing cutter and remove component from unit.
d. Carefully unsweat remaining tubing stubs when necessary. Oil can ignite when exposed to torch flame.

Use the Start-Up Checklist supplied at the end of this book and proceed as follows to inspect and prepare the unit for initial start-up:

1. Remove access panels (see Fig. 24).
2. Read and follow instructions on all DANGER, WARNING, CAUTION, and INFORMATION labels attached to, or shipped with unit.
3. Make the following inspections:
a. Inspect for shipping and handling damage, such as broken lines, loose parts, disconnected wires, etc.
b. Inspect all field- and factory-wiring connections. Be sure that connections are completed and tight.
c. Ensure wires do not touch refrigerant tubing or sharp sheet metal edges.
d. Inspect coil fins. If damaged during shipping and handling, carefully straighten fins with a fin comb.

## 4 WARNING

## FIRE, EXPLOSION HAZARD

Failure to follow this warning could result in personal injury, death or property damage.
Do not purge gas supply into the combustion chamber. Do not use a match or other open flame to check for gas leaks. Use a commercially available soap solution made specifically for the detection of leaks to check all connections. A fire or explosion may result causing property damage, personal injury or loss of life.
4. Verify the following conditions:
a. Make sure gas line is free of air. Before lighting the unit for the first time, perform the following with the gas valve in the OFF position:
NOTE: If the gas supply pipe was not purged before connecting the unit, it will be full of air. It is recommended that the ground joint union be loosened, and the supply line be allowed to purge until the odor of gas is detected. Never purge gas lines into a combustion chamber. Immediately upon detection of gas odor, retighten the union. Allow 5 minutes to elapse, then light unit.
b. Make sure that outdoor-fan blade is correctly positioned in the fan orifice.
c. Make sure that air filter(s) is in place.
d. Make sure that condensate drain trap is filled with water to ensure proper drainage.
e. Make sure that all tools and miscellaneous loose parts have been removed.

## START-UP

## Step 1 - Check for Refrigerant Leaks



## WARNING

## EXPLOSION HAZARD

Failure to follow this warning could result in death, serious personal injury, and/or property damage.
Never use air or gases containing oxygen for leak testing or operating refrigerant compressors. Pressurized mixtures of air or gases containing oxygen can lead to an explosion.

Proceed as follows to locate and repair a refrigerant leak and to charge the unit:

1. Locate leak and make sure that refrigerant system pressure has been relieved and reclaimed from both high- and low-pressure ports.
2. Repair leak following accepted practices.

NOTE: Install a filter drier whenever the system has been opened for repair.
3. Add a small charge of Puron (R-410A) refrigerant vapor to system and leak-test unit.
4. Recover refrigerant from refrigerant system and evacuate to 500 microns if no additional leaks are found.
5. Charge unit with Puron (R-410A) refrigerant, using an accurate scale. Refer to unit rating plate for required charge.

## Step 2 - Start-up Heating and Make Adjustments

Complete the required procedures given in the Pre-Start-Up section before starting the unit. Do not jumper any safety devices when operating the unit. Make sure that burner orifices are properly aligned. Unstable operation my occur when the burner orifices in the manifold are misaligned.
Follow the lighting instructions on the heating section operation label (located on the inside of the control access panel) to start the heating section.
NOTE: Make sure that gas supply has been purged, and that all gas piping has been checked for leaks.


Fig. 13 - Burner Assembly


Fig. 14 - Monoport Burner

## Check Heating Control

Start and check the unit for proper heating control operation as follows (see furnace lighting instructions located on the inside of the control access panel):

## For 208/230 VAC Models:

1. Place room thermostat SYSTEM switch in the HEAT position and the fan switch in AUTO position.
2. Set the heating temperature control setting several degrees higher than the room temperature reading.
3. The induced-draft motor will always start on high speed for the ignition sequence, regardless of the heating stage called.
4. After a pre-purge time of 15 sec with the induced-draft motor on high speed, the sparker will be energized for 3-to-8 sec , and the gas valve will be energized on low stage. If the burners do not light, there is a $20-$ sec delay before another ignition attempt. If the burners still do not light by the $4^{\text {th }}$ consecutive ignition attempt, there is a lockout. To reset the lockout, break the $24-\mathrm{v}$ power to W1 and W2.
5. Once flame is established the integrated gas unit controller (IGC) will look for $24-\mathrm{v}$ power to W1 and W2. If there is $24-\mathrm{v}$ power to W1 only, the IGC will switch the induceddraft motor down to low speed and maintain low stage on the gas valve. If there is $24-\mathrm{v}$ power to both W1 and W2, the IGC will maintain the induced-draft motor on high speed and switch the gas valve to high stage.
6. With the desired temperature set several degrees higher than the room temperature, most thermostats will energize low and high stage. Verify that the gas valve is energized on high stage and the induced-draft motor is on high speed.
7. Verify proper operation of low stage (induced-draft motor on low speed and gas valve on high stage) by turning the heating temperature control setting down until the desired temperature is 1 degree above room temperature. Most thermostats will energize low stage only with a 1 degree differential.
8. The evaporator fan will turn on 30 sec after the flame has been established. If there is $24-\mathrm{v}$ power to W1 only, the fan will run on low heat speed. If there is $24-\mathrm{v}$ power to W 1 and W2, the fan will run on high heat speed. Once the heating coll is satisfied, the IGC will turn the fan off after a field-selectable fan delay of $90,120,150$, or 180 sec is completed.

## For 460 VAC Models:

1. Place room thermostat SYSTEM switch in the HEAT position and the fan switch is placed in AUTO position.
2. Set the heating temperature control of the thermostat above room temperature.
3. The induced-draft motor will start.
4. On a call for heating, the main burner should light within 5 sec of the spark being energized. If the burners do not light, there is a $22-\mathrm{sec}$ delay before another $5-\mathrm{sec}$ try. If the burners still do not light, this sequence is repeated. If the burners do not light within 15 minutes from the initial call for heat, there is a lockout. To reset the control, break the 24 -v power to W .
5. The evaporator fan will turn on 45 sec after the flame has been established. The evaporator fan will turn off 45 sec after the thermostat has been satisfied. Please note that the integrated gas unit controller (IGC) has the capability to automatically reduce the evaporator "ON" delay and increase the evaporator "OFF" delay in the event of high duct static and/or partially-clogged filter.

## Check Gas Input

Check gas input and manifold pressure after unit start-up (See Table 6 or 7). If adjustment is required proceed as follows:

- The rated gas inputs shown in Table 6 or 7 are for altitudes from sea level to $2000 \mathrm{ft}(610 \mathrm{~m})$ above sea level. These inputs are based on natural gas with a heating value of $1025 \mathrm{Btu} / \mathrm{ft}^{3}$ at 0.60 specific gravity, or propane gas with a heating value of 2500 Btu/ft ${ }^{3}$ at 1.5 specific gravity.

IN THE U.S.A.:
The input rating for altitudes above $2,000 \mathrm{ft}(610 \mathrm{~m})$ must be reduced by $4 \%$ for each $1,000 \mathrm{ft}(305 \mathrm{~m}$ ) above see level.
For installations below 2,000 $\mathrm{ft}(610 \mathrm{~m}$ ), refer to the unit rating plate.
For installations above $2,000 \mathrm{ft}(610 \mathrm{~m})$. multiply the input on the rating plate by the derate multiplier in Table 3 for correct input rate. If the natural gas is not derated by the gas utility company, refer to Table 4 (208/230 VAC models) or Table 5 ( 460 VAC models) for correct orifice sizes and manifold pressures.

Table 3 - Altitude Derate Multiplier for U.S.A.*

| ALTITUDE FT (M) | PERCENT OF DERATE | DERATE MULTIPLIER FACTOR $\dagger$ |
| :---: | :---: | :---: |
| $\begin{aligned} & 0-2000 \\ & (0-610) \end{aligned}$ | 0 | 1.00 |
| $\begin{gathered} 2001-3000^{*} \\ (610-914) \end{gathered}$ | 8-12 | 0.90 |
| $\begin{aligned} & 3001-4000 \\ & (915-1219) \end{aligned}$ | 12-16 | 0.86 |
| $\begin{gathered} 4001-5000 \\ (1220-1524) \end{gathered}$ | 16-20 | 0.82 |
| $\begin{gathered} 5001-6000 \\ (1524-1829) \end{gathered}$ | 20-24 | 0.78 |
| $\begin{gathered} 6001-7000 \\ (1829-2134) \end{gathered}$ | 24-28 | 0.74 |
| $\begin{gathered} 7001-8000 \\ (2134-2438) \end{gathered}$ | 28-32 | 0.70 |
| $\begin{gathered} 8001-9000 \\ (2439-2743) \end{gathered}$ | 32-36 | 0.66 |
| $\begin{aligned} & 9001-10,000 \\ & (2744-3048) \end{aligned}$ | 36-40 | 0.62 |

*In Canada see Canadian Altitude Adjustment.
$\dagger$ Derate multiplier factors are based on midpoint altitude for altitude range.

## IN CANADA:

The input rating for altitudes from 2,000 ( 610 m ) to $4,500 \mathrm{ft}(1372$ m ) above sea level must be derated $10 \%$ by an authorized Gas Conversion Station or Dealer.

## EXAMPLE:

$90,000 \mathrm{Btu} / \mathrm{hr}$ Input Furnace Installed at 4300 ft .

| Furnace Input Rate at <br> Sea Level | XDerate Multiplier <br> Factor | $=$Furnace Input Rate at <br> Installation Altitude |  |
| :---: | :---: | :---: | :---: |
| 90,000 | X | 0.90 | $=$ |

When the gas supply being used has a different heating value or specific gravity, refer to national and local codes, or contact your distributor to determine the required orifice size.


## UNIT DAMAGE HAZARD

Failure to follow this caution may result in reduced unit and/or component life.
Do Not redrill an orifice. Improper drilling (burrs, out-of-round holes, etc.) can cause excessive burner noise and misdirection of burner flame. If orifice hole appears damaged or it is suspected to have been redrilled, check orifice hole with a numbered drill bit of correct size.

## Adjust Gas Input

The gas input to the unit is determined by measuring the gas flow at the meter or by measuring the manifold pressure. Measuring the gas flow at the meter is recommended for natural gas units. The manifold pressure must be measured to determine the input of propane gas units.

## Measure Gas Flow (Natural Gas Units)

Minor adjustment to the gas flow can be made by changing the manifold pressure(s). The manifold pressure(s) must be maintained between 3.2 and 3.8 IN. W.C. for high stage and between 1.4 and 2.0 IN. W.C. for low stage (208/230 VAC models). For 460 VAC models, manifold pressure must be maintained between 3.2 and 3.8 IN. W.C.

Table 4 - Natural Gas Orifice Sizes and Manifold Pressure
208/230VAC Models

| Nameplate <br> Input, <br> High Stage <br> (Btu/hr) |  | ALTITUDE OF INSTALLATION (FT. [m] ABOVE SEA LEVEL) U.S.A.* |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |

Table 5 - Natural Gas Orifice Sizes and Manifold Pressure
460V

| $\begin{array}{c}\text { Nameplate } \\ \text { Input } \\ \text { (Btu/hr) }\end{array}$ |  | ALTITUDE OF INSTALLATION (FT. ABOVE SEA LEVEL) U.S.A.* |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |$]$

$\star$ In the U.S.A., the input rating for altitudes above $2000 \mathrm{ft}(610 \mathrm{~m})$ must be reduced by $4 \%$ for each $1000 \mathrm{ft}(305 \mathrm{~m})$ above sea level.
In Canada, the input rating for altitudes from 2001 to $4500 \mathrm{ft}(611$ to 1372 m ) above sea level must be derated by $10 \%$ by an authorized gas conversion station or dealer.
For Canadian Installations from 2000 to 4500 ft , use U.S.A. column 2001 to 3000 ft ( 610 to 914 m ).
$\dagger$ Orifices available through your distributor.
NOTE: Orifice sizes and manifold pressure settings are based on natural gas with a heating value of $1025 \mathrm{Btu} / \mathrm{ft}^{3}$ and a specific gravity of .6 .


A04167
Fig. 15 - Two-Stage Gas Valve (208/230 VAC Models)

A07751
Fig. 16 - Single-Stage Gas Valve ( 460 VAC Models)
If larger adjustments are required, change main burner orifices following the recommendations of national and local codes.
NOTE: All other appliances that use the same meter must be turned off when gas flow is measured at the meter.
Proceed as follows:

1. Turn off gas supply to unit.
2. Remove pipe plug on manifold (See Fig. 13) and connect manometer. Turn on gas supply to unit.
3. Record number of seconds for gas meter test dial to make one revolution.
4. Divide number of seconds in Step 3 into 3600 (number of seconds in one hr).
5. Multiply result of Step 4 by the number of cubic feet (cu ft) shown for one revolution of test dial to obtain cubic feet (cu ft ) of gas flow per hour.
6. Multiply result of Step 5 by Btu heating value of gas to obtain total measured input in Btuh. Compare this value with heating input shown in Table 6 or 7 (Consult the local gas supplier if the heating value of gas is not known).
EXAMPLE: Assume that the size of test dial is 1 cu ft , one revolution takes 32 sec and the heating value of the gas is 1050 Btu/ft ${ }^{3}$. Proceed as follows:
7. 32 sec to complete one revolution.
8. $3600 \div 32=112.5$.
9. $112.5 \times 1=112.5 \mathrm{ft}^{3}$ of gas flow $/ \mathrm{hr}$.
10. $112.5 \times 1050=118,125$ Btuh input.

If the desired gas input is 115,000 Btuh, only a minor change in the manifold pressure is required.
Observe manifold pressure(s) and proceed as follows to adjust gas input(s):

1. Remove regulator cover screw(s) over plastic adjustment screw(s) on gas valve (Fig. 15 For 208/230 VAC models, Fig. 16 For 460 VAC models).
2. For 208/230 VAC models only: Turn the high stage plastic adjustment screw clockwise to increase gas input and counterclockwise to decrease input (see Fig. 15). For 460 VAC models only: Turn the plastic adjustment screw clockwise to increase gas input and counterclockwise to decrease input (see Fig. 16). Manifold pressure must be between 3.2 and 3.8 IN. W.C. For high stage on 208/230 VAC models and for single stage on 460 VAC models.
3. For 208/230 VAC models only: Replace high stage regulator cover screw on gas valve (see Fig. 15). For 460 VAC models only: Replace regulator cover screw on gas valve (See Fig. 16).
4. For 208/230 VAC models only: turn the low stage plastic adjustment screw clockwise to increase gas input and counterclockwise to decrease input (see Fig. 15). Low stage manifold pressure must be between 1.4 and 2.0 IN. W.C.
NOTE: For 208/230 VAC models only, low stage manifold pressure must be adjusted after high stage manifold pressure is already adjusted.
5. For 208/230 VAC models only: Replace low stage regulator cover screw(s) on gas valve (see Fig. 15).
6. Turn off gas supply to unit. Remove manometer from pressure tap and replace pipe plug on manifold (see Fig. 13). Turn on gas and check for leaks

## WARNING

## FIRE AND UNIT DAMAGE HAZARD

Failure to follow this warning could result in personal injury or death and/or property damage.
Unsafe operation of the unit may result if manifold pressure is outside this range.

## Measure Manifold Pressure (Propane Units)

Refer to propane kit installation instructions for properly checking gas input.
NOTE: For installations below $2,000 \mathrm{ft}(610 \mathrm{~m})$, refer to the unit rating plate for proper propane conversion kit. For installations above $2,000 \mathrm{ft}(610 \mathrm{~m})$, contact your distributor for proper propane conversion kit.

## Check Burner Flame

With control access panel (see Fig. 24) removed, observe the unit heating operation. Watch the burner flames to see if they are light blue and soft in appearance, and that the flames are approximately the same for each burner. Propane will have blue flame (See Fig. 14). Refer to the Maintenance section for information on burner removal.

Table 6 - Heating Inputs 208/230 VAC Models

| HEATING INPUT (BTUH) | NUMBER OF ORIFICES | GAS SUPPLY PRESSURE (IN. W.C.) |  |  |  | MANIFOLD PRESSURE <br> (IN. W.C.) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Natural $\dagger$ |  | Propane* $\dagger$ |  |  |  |
|  |  | Min | Max | Min | Max | Natural $\dagger$ | Propane*† |
| 40,000 | 2 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |
| 60,000 | 2 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |
| 90,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |
| 115,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |
| 127,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |
| 130,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 |

*When a unit is converted to propane, different size orifices must be used. See separate, natural-to-propane conversion kit instructions.
$\dagger$ Based on altitudes from sea level to $2000 \mathrm{ft}(610 \mathrm{~m})$ above sea level. In U.S.A. for altitudes above $2000 \mathrm{ft}(610 \mathrm{~m})$, reduce input rating 4 percent for each additional $1000 \mathrm{ft}(305 \mathrm{~m})$ above sea level. In Canada, from $2000 \mathrm{ft}(610 \mathrm{~m})$ above sea level to $4500 \mathrm{ft}(1372 \mathrm{~m})$ above sea level, derate the unit 10 percent.

Table 7 - Heating Inputs, 460 VAC Models

| HEATING INPUT, HIGH STAGE (BTUH) | NUMBER OF ORIFICES | GAS SUPPLY PRESSURE (IN. W.C.) |  |  |  | MANIFOLD PRESSURE (IN. W.C.) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Natural $\dagger$ |  | Propane*† |  | HIGH STAGE |  | LOW STAGE |  |
|  |  | Min | Max | Min | Max | Natural $\dagger$ | Propane* $\dagger$ | Natural $\dagger$ | Propane*† |
| 40,000 | 2 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 | 1.4~2.0 | 4.8~6.4 |
| 60,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 | 1.4~2.0 | 4.8~6.4 |
| 90,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 | 1.4~2.0 | 4.8~6.4 |
| 115,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 | 1.4~2.0 | 4.8~6.4 |
| 130,000 | 3 | 4.0 | 13.0 | 11.0 | 13.0 | 3.2~3.8 | 10.0~11.0 | 1.4~2.0 | 4.8~6.4 |

*When a unit is converted to propane, different size orifices must be used. See separate, natural-to-propane conversion kit instructions.
$\dagger$ Based on altitudes from sea level to $2000 \mathrm{ft}(610 \mathrm{~m})$ above sea level. In U.S.A. for altitudes above $2000 \mathrm{ft}(610 \mathrm{~m})$, reduce input rating 4 percent for each additional $1000 \mathrm{ft}(305 \mathrm{~m})$ above sea level. In Canada, from $2000 \mathrm{ft}(610 \mathrm{~m})$ above sea level to $4500 \mathrm{ft}(1372 \mathrm{~m})$ above sea level, derate the unit 10 percent.

## CONNECTION WIRING DIAGRAM

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING
SCHEMATIC 208/230-1-60


Fig. 17-208/230-1-60 Connection Wiring Diagram

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING


A14594
Fig. 17 Cont. - 208/230-1-60 Ladder Wiring Diagram

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING


A14615
Fig. 18-208/230-3-60 Connection Wiring Diagram Gas Inputs 40, 60, 90 KBtu/hr

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING

| LEGEND |  |  |  |
| :---: | :---: | :---: | :---: |
| $\triangle$ | FIELD SPLICE | $\begin{aligned} & \text { EOUIP } \\ & \text { FSND } \\ & \text { GND } \\ & \text { HPS } \end{aligned}$ | EQUIPMENT FLAME SENSOR |
| $\square$ | TERMINAL (MARKED) |  |  |
| - | TERMNAL (UNMARKED) |  | HIGH PRESSURE SWITCH |
| - | SPLCE | $\underset{\substack{\text { ITM } \\ \text { IFM }}}{\text { cic }}$ |  |
| $\bigcirc$ | SPLCE (MARKED) |  | INDOOR FAN MOTOR |
|  | FACTORY LO VOLTAGE FIELD CONTROL WRING ACCESSORY OR OPTIONAL WRING | LGPS | NTERGRATED GAS UNT CONTROLER LOW GAS PRESSURE SWITCH (WHEN USED) |
|  |  |  | LOW PRESSURE SWTCH |
|  |  | ${ }_{\text {LS1 }}^{\text {LS1 }}$ | PRMARY LMMT SWITCH |
|  |  | MGV | MAIN GAS Valve |
| - | FACTORY HIV VOLTAGE | $\begin{aligned} & \text { OFM } \\ & \text { OT } \end{aligned}$ | OUTDOOR FAN MOTOR |
| ${ }_{\text {c }}^{\text {CAP1 }}$ | CONACTOR ${ }_{\text {CAPACTOR, }}$ COMP |  | QUADRUPLE TERMMAL IGC TO NDUCER MOTOR PLUG |
| ( ${ }_{\text {CAP2 }}$ | CAPACCITOR, INOUCER | ${ }_{\text {RS }} \mathrm{P}$ 2 | INDUCER MOTOR PlUG |
|  | CRANKCASE HEATER |  | ROLLOUT SWITCH |
| COMP | COMPRESSOR MOTOR | SOL | COMPRESSOR SOLENOID |
|  |  | ${ }_{\text {Trestat }}^{\text {T-SAT }}$ | THANSORMER THERMOSTAT |

$3 \varnothing$ UNIT COMPONENT ARRANGEMENT


## NOTES:

1. IF ANY OF THE ORIGINAL WIRES FURNISHED ARE REPLACED THEY MUST BE REPLACED WITH THE SAME WIRE OR IT'S EQUIVALENT. 2. SEE PRE-SALE LITERATURE FOR THERMOSTATS.
2. USE 75 DEGREES C COPPER CONDUCTORS FOR FIELD INSTALLATION.
3. REFER TO INSTALLATION INSTRUCTIONS FOR CORRECT SPEED SELECTION FOR IFM.
4. SEE INSTALLATION INSTRUCTIONS FOR PROPER HEATING AND COOLING CONNECTIONS FOR YOUR UNIT.
5. ON SOME MODELS LS1 AND LS2 ARE WIRED IN SERIES. ON OTHER MODELS ONLY LS1 IS USED
6. THIS FUSE IS MANUFACTURED BY LITTLE FUSE, P/N 257003.
7. DO NOT DISCONNECT PLUG UNDER LOAD.
8. N.E.C. CLASS $2,24 \mathrm{~V}$.


Fig. 18 Cont. - 208/230-3-60 Ladder Wiring Diagram Gas Inputs 40, 60, 90 KBtu/hr

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING


Fig. 19-208/230-3-60 Connection Wiring Diagram Gas Inputs 115, 130

LADDER WIRING DIAGRAM
DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING


Fig. 19 Cont. - 208/230-3-60 Ladder Wiring Diagram Gas Inputs 115, 130

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING


Fig. 20-460-3-60 Connection Wiring Diagram

DANGER: ELECTRICAL SHOCK HAZARD DISCONNECT POWER BEFORE SERVICING

| LEGEND |  |  |  |
| :---: | :---: | :---: | :---: |
| $\triangle$ | FIELD SPLICE | FS | FLAME SENSOR |
| $\square$ | TERMINAL (MARKED) | GND HPS | GROUND |
| $\bigcirc$ | TERMINAL (UNMARKED) | HPS | IGNITOR |
| $\bullet$ | SPLICE | IFB | INDOOR FAN BOARD |
| $\bigcirc$ | SPLICE (MARKED) | $\begin{aligned} & \text { IGC } \\ & \text { IחM } \end{aligned}$ | INTERGRATED GAS UNIT CONTROLLER INDUCED DRAFT MOTOR |
|  | FACTORY LO VOLTAGE | IFM | INDOOR FAN MOTOR |
| - - | FIELD CONTROL WIRING | LGPS | LOW GAS PRESSURE SWITCH |
|  | FIEID POWER WIRING | LPS | LOW PRESSURE SWITCH |
|  | FIELD POWER WIRING | LS1 | PRIMARY LIMIT SWITCH |
|  | ACCESSORY OR OPTIONAL WIRING | $\begin{aligned} & \text { LS2 } \\ & \text { MGV } \end{aligned}$ | SECONDARY LIMIT SWITCH MAIN GAS VALVE |
|  | FACTORY HI VOLTAGE | OFM | OUTDOOR FAN MOTOR |
| C | CONTACTOR | PRS | PRESSURE SWITCH |
| CAP 1 | CAPACITOR, COMP | QS | QUADRUPLE TERMINAL |
| CAP 2 | CAPACITOR, INDUCER | RS | COMPRESSOR SOLENOID |
| COMP | COMPRESSOR MOTOR | TRAN | TRANSFORMER |
| CCH | CRANK CASE HEATER | T-STAT | THERMOSTAT |




$3 \varnothing$ UNIT COMPONENT ARRANGEMENT


## NOTES:

1. IF ANY OF THE ORIGINAL WIRES FURNISHED ARE REPLACED, THEY MUST BE REPLACED WITH THE SAME WIRE OR IT'S EQUIVALENT.
2. SEE PRE SALE LITERATURE FOR THERMOSTAT.
3. USE 75 DEGREE COPPER CONDUCTORS FOR FIELD INSTALLATION
4. SEE INSTALLATION INSTRUCTIONS FOR PROPER HEATING AND COOLING CONNECTIONS FOR YOUR UNIT.
5. LS2 USED ON SMALL CHASSIS ONLY
6. INDUCER CAPACITOR AND WIRING ON CERTAIN MODELS ONLY. IF CAP2 IS PRESENT,
7. INDUCER CAPACIIOR AND WIRING ON CERTAIN MODELS ON SAM ID CIDE OF CAP2.
8. THIS FUSE IS MANUFACTURED BY LITTLE FUSE, P/N 287003.
9. THIS FUSE IS MANUFACTURED BY LITTLEFUSE, P/N 257005.
10. ON SOME MODELS LS1 AND LS2 ARE WIRED IN SERIES. ON OTHER MODELS ONLY LS1 IS USED.
11. DO NOT DISCONNECT PLUG UNDER LOAD.

Fig. 20 Cont.- 460-3-60 Ladder Wiring Diagram

## Normal Operation

An LED (light-emitting diode) indicator is provided on the integrated gas unit controller (IGC) to monitor operation. The IGC is located by removing the control access panel (see Fig. 24). During normal operation, the LED is continuously on (See Table 8 for error codes).

## Airflow and Temperature Rise

The heating section for each size unit is designed and approved for heating operation within the temperature-rise range(s) stamped on the unit rating plate.
Tables 14 and 15 show the approved temperature rise range for each heating input and stage, and the air delivery cfm at various temperature rises for a given external static pressure. The heating operation airflow must produce a temperature rise that falls within the approved range for each heating stage.
Refer to Indoor Airflow and Airflow Adjustments section to adjust heating airflow when required.

## Heating Sequence of Operation

(See Fig. 17, 18, 19 and unit wiring label.)

## 208/230 VAC Models:

On a call for low stage heating, terminal W1 on the thermostat is energized. On a call for high stage heating both terminals W1 and W2 are energized. Regardless of the stage of the heating call, the induced-draft motor is turned on to high speed for a 15 sec pre-purge time. After the pre-purge, when the pressure switch senses that sufficient combustion air is being moved by the induced-draft motor, the ignition sequence begins. The IGC will energize the sparker and the low stage gas valve solenoid. Upon sensing flame, the IGC will check the heating call. If W2 is not energized, the IGC will drop the induced-draft motor to low speed and maintain the gas valve on low stage. If W2 is energized, the IGC will maintain the induced-draft motor on high speed and energize the high stage gas valve solenoid. Thirty sec after flame is sensed the IGC will turn on the evaporator fan motor. If W2 is not energized, the evaporator fan motor will run on low heat speed. If W2 is energized, the evaporator fan motor will run on high heat speed. After the call for heat is satisfied, the IGC will run the evaporator fan motor an additional field-selectable time of 90,120 , 150 , or 180 sec before shutting the evaporator fan motor off.

## 460 VAC Models:

On a call for heating, terminal W of the thermostat is energized, starting the induced-draft motor. When the pressure switch senses that the induced-draft motor is moving sufficient combustion air, the ignition sequence begins. This function is performed by the integrated gas unit controller (IGC). The indoor (evaporator)-fan motor is energized 45 sec after flame is established. When the thermostat is satisfied and W is de-energized, the burners stop firing and the indoor (evaporator) fan motor shuts off after a 45 -sec time-off delay. Please note that the IGC has the capability to automatically reduce the indoor fan motor on delay and increase the indoor fan motor off delay in the event of high duct static and/or partially-clogged filter.

## Limit Switches

Normally closed limit switch(es) (LS) complete the control circuit. Should the leaving-air temperature rise above the maximum allowable temperature, the limit switch opens and the control circuit "breaks." Any interruption in the control circuit instantly closes the gas valve and stops gas flow to the burners. The blower motor continues to run until LS resets.
When the air temperature at the limit switch drops to the low-temperature setting of the limit switch, the switch closes and completes the control circuit. The direct-spark ignition system cycles and the unit returns to normal heating operation.

Table 8 - LED Indications

| STATUS CODE | LED INDICATION |
| :---: | :---: |
| Normal Operation ${ }^{\mathbf{2}}$ | On |
| No Power or Hardware Failure | Off |
| Check Fuse, Low Voltage Circuit | 1 Flash |
| Limit Switch Fault | 2 Flashes |
| Flame Sense Fault | 3 Flashes |
| Four Consecutive Limit Switch Faults | 4 Flashes |
| Ignition Lockout Fault | 5 Flashes |
| Pressure Switch Fault | 6 Flashes |
| Rollout Switch Fault | 7 Flashes |
| Internal Control Fault | 8 Flashes |
| Temporary 1 hr auto reset ${ }^{\mathbf{1}}$ | 9 Flashes |

NOTES:
1.This code indicates an internal processor fault that will reset itself in one hr. Fault can be caused by stray RF signals in the structure or nearby. This is a UL requirement.
2. LED indicates acceptable operation. Do not change ignition control board.
3. When W is energized the burners will remain on for a minimum of 60 sec . 4. If more than one error code exists they will be displayed on the LED in sequence.

## Rollout Switch

The function of the rollout switch is to close the main gas valve in the event of flame rollout. The switch is located above the main burners. When the temperature at the rollout switch reaches the maximum allowable temperature, the control circuit trips, closing the gas valve and stopping gas flow to the burners. The indoor (evaporator) fan motor (IFM) and induced draft motor continue to run until switch is reset. The IGC LED will display FAULT CODE 7.

## Step 3 - Start-up Cooling and Make Adjustments

Complete the required procedures given in the Pre-Start-Up section before starting the unit. Do not jumper any safety devices when operating the unit. Do not operate the compressor when the outdoor temperature is below $40^{\circ} \mathrm{F}\left(4.4^{\circ} \mathrm{C}\right)$ (unless accessory low-ambient kit is installed). Do not rapid-cycle the compressor. Allow 5 minutes between on cycles to prevent compressor damage.

## Checking Cooling Control Operation

Start and check the unit for proper control operation as follows:

1. Place room thermostat SYSTEM switch or MODE control in OFF position. Observe that blower motor starts when FAN mode is placed in FAN ON position and shuts down when FAN MODE switch is placed in AUTO position.
2. Thermostat:

On a typical two stage thermostat, when the room temperature rises 1 or 2 degrees above the cooling control setting of the thermostat, the thermostat completes the circuit between thermostat terminal R and terminals Y1, and G. These completed circuits through the thermostat connect the contactor coil (C) (through unit wire Y1) and indoor fan board (through unit wire G) across the $24-\mathrm{v}$. secondary of transformer (TRAN).
On a typical two stage thermostat, when the room temperature is several degrees above the cooling control setting of the thermostat, the thermostat completes the circuit between terminal R and terminals $\mathrm{T} 1, \mathrm{Y} 2$, and G .
3. When using an automatic changeover room thermostat place both SYSTEM or MODE control and FAN mode stitches in AUTO positions. Observe that unit operates in Cooling mode when temperature control is set to "call for Cooling" (below room temperature).
NOTE: Once the compressor has started and then has stopped, it should not be started again until 5 minutes have elapsed.
IMPORTANT: Three-phase, scroll compressors are direction oriented. Unit must be checked to ensure proper compressor

3-phase power lead orientation. If not corrected within 5 minutes, the internal protector will shut off the compressor. The 3-phase power leads to the unit must be reversed to correct rotation. When turning backwards, the difference between compressor suction and discharge pressures will be minimal.

## Checking and Adjusting Refrigerant Charge

The refrigerant system is fully charged with Puron ${ }^{\circledR}$ ( $\mathrm{R}-410 \mathrm{~A}$ ) refrigerant and is tested and factory sealed. Allow system to operate a minimum of 15 minutes before checking or adjusting charge.
NOTE: Adjustment of the refrigerant charge is not required unless the unit is suspected of not having the proper Puron ${ }^{\circledR}$ ( $\mathrm{R}-410 \mathrm{~A}$ ) charge.
A subcooling chart is attached to the inside of the compressor access panel. (See Table 12 and Fig. 24.) The chart includes the required liquid line temperature at given discharge line pressures and outdoor ambient temperatures for high stage cooling.
An accurate thermocouple- or thermistor-type thermometer, and a gauge manifold are required when using the subcooling charging method for evaluating the unit charge. Do not use mercury or small dial-type thermometers because they are not adequate for this type of measurement.

## 1 CAUTION

## UNIT DAMAGE HAZARD

Failure to follow this caution may result in unit damage.
When evaluating the refrigerant charge, an indicated adjustment to the specified factory charge must always be very minimal. If a substantial adjustment is indicated, an abnormal condition exists somewhere in the cooling system, such as insufficient airflow across either coil or both coils.

IMPORTANT: When evaluating the refrigerant charge, an indicated adjustment to the specified factory charge must always be very minimal. If a substantial adjustment is indicated, an abnormal condition exists somewhere in the cooling system, such as insufficient airflow across either coil or both coils.
Proceed as follows:

1. Remove caps from low- and high-pressure service fittings.
2. Using hoses with valve core depressors, attach low- and high-pressure gauge hoses to low- and high-pressure service fittings, respectively.
3. Start unit in high stage cooling mode and let unit run until system pressures stabilize.
4. Measure and record the following:
a. Outdoor ambient-air temperature $\left({ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right] \mathrm{db}\right)$.
b. Liquid line temperature $\left({ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right]\right)$.
c. Discharge (high-side) pressure (psig).
d. Suction (low-side) pressure (psig) (for reference only).
5. Using "Subcooling Charging Charts," compare outdoor-air temperature $\left({ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right] \mathrm{db}\right)$ with the discharge line pressure (psig) to determine desired system operating liquid line temperature (See Table 12).
6. Compare actual liquid line temperature with desired liquid line temperature. Using a tolerance of $\pm 2^{\circ} \mathrm{F}\left( \pm 1.1^{\circ} \mathrm{C}\right)$, add refrigerant if actual temperature is more than $2^{\circ} \mathrm{F}\left(1.1^{\circ} \mathrm{C}\right)$ higher than proper liquid line temperature, or remove refrigerant if actual temperature is more than $2^{\circ} \mathrm{F}\left(1.1^{\circ} \mathrm{C}\right)$ lower than required liquid line temperature.
NOTE: If the problem causing the inaccurate readings is a refrigerant leak, refer to the Check for Refrigerant Leaks section.

Indoor Airflow and Airflow Adjustments

## 4 CAUTION

## UNIT OPERATION HAZARD

Failure to follow this caution may result in unit damage.
For cooling operation, the recommended airflow is 350 to 450 cfm for each 12,000 Btuh of rated cooling capacity. For heating operation, the airflow must produce a temperature rise that falls within the range stamped on the unit rating plate.

NOTE: Be sure that all supply-and return-air grilles are open, free from obstructions, and adjusted properly.

## 4 WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.
Disconnect electrical power to the unit and install lockout tag before changing blower speed(s).

This unit has independent fan speeds for low stage cooling and high stage cooling. In addition, 208/230 VAC models have the field-selectable capability to run an enhanced dehumidification ('DHUM') speed on high stage cooling (as low as 320CFM per ton). Coupled with the improved dehumidification associated with low stage cooling, the DHUM speed allows for a complete dehumidification solution independent of cooling stage. 208/230 VAC models also have independent fan speeds for low stage gas heating and high stage gas heating. 460 VAC models offer a single gas heating speed. Table 9 and 10 show the operation modes and the associated fan speeds with each mode:

Table 9 - Operation Modes and Fan Speeds 208/230 VAC Models

| OPERATION MODE | FAN SPEED TAP <br> CONNECTION |
| :---: | :---: |
| Low Stage Gas Heating | LO HEAT |
| High Stage Gas Heating | HI HEAT |
| Low Stage Cooling | LO COOL |
| High Stage Cooling | HI COOL |
| High Stage Enhanced <br> Dehumidification Cooling | DHUM |
| Continuous Fan | LO COOL |

Table 10 - Operation Modes and Fan Speeds 460 VAC Models

| OPERATION MODE | FAN SPEED TAP <br> CONNECTION |
| :---: | :---: |
| Gas Heating | GAS HEAT |
| Low Stage Cooling | LOW |
| High Stage Cooling | HIGH |
| Continuous Fan | LOW |

The evaporator fan motor is factory set to provide 5 different fan speeds to choose from for the various operation modes. 208/230 VAC models are factory-shipped with 4 speed wires connected with one spare speed wire available. 460 VAC models are
factory-shipped with 3 speed wires connected and 2 speed wires available. The fan speed wires are color-coded as follows:

Table 11 - Color Coding for Indoor Fan Motor Leads

| Black $=$ High Speed |
| :---: |
| Orange $=$ Med - High Speed |
| Red $=$ Med Speed |
| Pink $=$ Med - Low Speed |
| Blue $=$ Low Speed |

## Selection of Proper Fan Speeds for Operation Modes:

NOTE: All models are factory-shipped for nominal high stage and low stage cooling airflow operation at minimum external static pressure. Many models are factory-shipped for nominal high stage and/or low stage gas heating airflow at minimum external static pressure. Tables 13, 14 (208/230 VAC models) and 15 ( 460 VAC models) provide airflow data for higher external static pressures.
Low Stage Gas Heating (208/230 VAC models): Table 13 and 14 show the suitability of each speed for a given external static pressure for low stage gas heating. Any speed/static combination that is outside the rise range is marked "NA" and must not be used. The unit must operate within the low stage gas heat rise range printed on the rating plate. Connect the chosen fan speed wire to "LO HEAT" connection on the IGC Board (see Fig. 21).
High Stage Gas Heating (208/230 VAC models): Table 13 and 14 show the suitability of each speed for a given external static pressure for high stage gas heating. Any speed/static combination that is outside the rise range is marked "NA" and must not be used. The unit must operate within the high stage gas heat rise range printed on the rating plate. Connect the chosen fan speed wire to "HI HEAT" connection on the IGC Board (see Fig. 21).
Gas Heating ( $\mathbf{4 6 0}$ VAC models): Table 15 shows the suitability of each speed for a given external static pressure for gas heating operation. Any speed/static combination that is outside the rise range is marked "NA" and must not be used. The unit must operate within the gas heat rise range printed on the rating plate. Connect the chosen fan speed wire to "GAS HEAT" connection on the Interface Fan Board (IFB, See Fig. 22).
Low Stage Cooling (All models): Using Tables 16, 17, and 18, and the nominal airflow for low stage cooling (Table 1) find the external static pressure drops for wet coil, economizer, and filter, and add them to dry coil measured on the system. Using this total static pressure, use Table 13 or 14 (208/230 VAC models) and Table 15 ( 460 VAC models) to find the airflows available at the total static pressure. For 208/230 VAC models, connect the chosen fan speed wire to "LO COOL" connection on the IGC Board (see Fig. 21). For 460 Vac models, connect the chosen fan speed wire to "LOW" connection on the IFB (see Fig. 22).
High Stage Cooling (All models)Using Tables 16, 17, and 18, find the external static pressure drops for wet coil, economizer, and filter, and add them to dry coil measured on the system. Using this total static pressure, use Table 13 or 14 (208/230 VAC models) and Table 15 ( 460 VAC models) to find the airflows available at the total static pressure. The speed chosen must provide airflow of between 350 to 450 CFM per ton of cooling. For 208/230 VAC models, connect the chosen fan speed wire to "HI COOL" connection on the IGC Board (See Fig. 21). For 460 VAC models, connect the chosen fan speed wire to "HIGH" connection on the IFB (see Fig. 22).
High Stage Enhanced Dehumidification Cooling (208/230 VAC Models): Using the total static pressure for selecting the high stage cooling speed, use Table 13 or 14 to find lower speed/airflows
available at that total static pressure. All airflows highlighted in Table 13 and 14 are acceptable for Dehum speed. The speed chosen must provide airflow of between 320 to 400 CFM per ton of cooling. For 208/230 VAC models, connect the chosen fan speed wire to "DHUM" connection on the IGC Board (see Fig. 21).

To activate the high stage enhanced dehumidification cooling mode, the shunt jumper in Fig. 21 must be moved from the No DH to DH selection (See Fig. 21, close up).
Continuous Fan (All models): Continuous fan speed is the same speed as Low Stage Cooling.
Using the Same Fan Speed for More than One Mode: Some fan speeds are ideal for more than one mode of operation. It is permissible to use a field-supplied jumper wire to connect one speed tap wire to two or more speed connections on the ignition board (IGC). Jumper wires must use 18 AWG wire with at least 2/64" insulation.

## Cooling Sequence of Operation

a. Continuous Fan
(1.) Thermostat closes circuit R to G energizing the blower motor for continuous fan. The indoor fan is energized on low speed.
b. Cooling Mode
(1.) Low Stage: Thermostat closes R to G, R to Y1. The compressor and indoor fan are energized on low speed. The outdoor fan is also energized.
(2.) High Stage: Thermostat closes R to G, R to Y1, R to Y2. The compressor and indoor fan are energized on high speed. The outdoor fan is also energized.


A13017
Fig. 21 - Interface Fan Board (IFB) 208/230 VAC Models


Fig. 22 - Interface Fan Board (IFB) 460 VAC Models
Table 12 - Subcooling Charging Chart


A12578

| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNAL | ATIC | ESS | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 24040 | 25-55야 Low Stage, 25-55ºF High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & \hline 27 \\ & (15) \end{aligned}$ | $\begin{aligned} & 37 \\ & (21) \end{aligned}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 42 \\ (23) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 689 | 597 | 489 | 352 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.06 | 0.06 | 0.05 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & \hline 28 \\ & (16) \end{aligned}$ | $\begin{aligned} & 33 \\ & (18) \end{aligned}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 43 \\ & (24) \\ & \hline \end{aligned}$ | $\begin{aligned} & 50 \\ & \text { (28) } \end{aligned}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 743 | 694 | 628 | 563 | 497 | 426 | 300 | --- | --- | --- |
|  |  |  |  | BHP | 0.12 | 0.13 | 0.13 | 0.13 | 0.14 | 0.15 | 0.15 | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & \hline 26 \\ & (15) \end{aligned}$ | $\begin{aligned} & \hline 28 \\ & (16) \end{aligned}$ | $\begin{aligned} & \hline 31 \\ & (17) \end{aligned}$ | $\begin{aligned} & \hline 35 \\ & (19) \\ & \hline \end{aligned}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 921 | 829 | 754 | 663 | 582 | 485 | 371 | --- | --- | --- |
|  |  |  |  | BHP | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 | 0.17 | 0.18 | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | High | Black | CFM | 1291 | 1206 | 1142 | 1081 | 1017 | 951 | 888 | 823 | 753 | 668 |
|  |  |  |  | BHP | 0.31 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | $\begin{aligned} & \hline 26 \\ & (14) \end{aligned}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 25 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 26 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNA | ATIC | SS | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 24060 | 25-55º Low Stage, 25-55º High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 689 | 597 | 489 | 352 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.06 | 0.06 | 0.05 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{aligned} & \hline 49 \\ & (27) \\ & \hline \end{aligned}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 921 | 829 | 754 | 663 | 582 | 485 | 371 | --- | --- | --- |
|  |  |  |  | BHP | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 | 0.17 | 0.18 | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1229 | 1171 | 1105 | 1049 | 980 | 913 | 838 | 775 | 679 | 516 |
|  |  |  |  | BHP | 0.28 | 0.30 | 0.30 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.34 | 0.33 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{aligned} & 27 \\ & (15) \end{aligned}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 37 \\ & (20) \end{aligned}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{aligned} & 41 \\ & (23) \end{aligned}$ | $\begin{aligned} & 43 \\ & (24) \end{aligned}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  | High | Black | CFM | 1291 | 1206 | 1142 | 1081 | 1017 | 951 | 888 | 823 | 753 | 668 |
|  |  |  |  | BHP | 0.31 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{aligned} & 27 \\ & (15) \end{aligned}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (26) \\ \hline \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \\ & \hline \end{aligned}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | NA | NA |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNA | ATIC | ESSU | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 30040 | 25-55º Low Stage, 25-55º F High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 831 | 765 | 670 | 586 | 466 | 299 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 33 \\ (19) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 831 | 765 | 670 | 586 | 466 | 299 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{aligned} & 26 \\ & (14) \end{aligned}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 33 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{aligned} & 39 \\ & (22) \end{aligned}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \end{aligned}$ | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1139 | 1069 | 1012 | 937 | 870 | 786 | 724 | 626 | 512 | 381 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | $\begin{aligned} & 25 \\ & (14) \end{aligned}$ | $\begin{aligned} & 27 \\ & (15) \end{aligned}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{aligned} & 38 \\ & 21) \end{aligned}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 26 \\ & (15) \\ & \hline \end{aligned}$ | $\begin{aligned} & 28 \\ & (16) \end{aligned}$ | $\begin{array}{r} 30 \\ (16) \\ \hline \end{array}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 38 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{aligned} & 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 48 \\ & (27) \end{aligned}$ | NA | NA |
|  |  | High | Black | CFM | 1531 | 1460 | 1382 | 1301 | 1209 | 1114 | 1003 | 890 | 764 | 629 |
|  |  |  |  | BHP | 0.53 | 0.52 | 0.50 | 0.48 | 0.46 | 0.44 | 0.42 | 0.40 | 0.37 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | $\begin{gathered} \hline 26 \\ (14) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 31 \\ & (17) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{aligned} & 27 \\ & (15) \end{aligned}$ | $\begin{aligned} & 30 \\ & (17) \end{aligned}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{aligned} & 39 \\ & (22) \end{aligned}$ | $\begin{gathered} 48 \\ (26) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNAL | ATIC | ESSU | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 30060 | 25-55야 Low Stage, 25-55ºF High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 831 | 765 | 670 | 586 | 466 | 299 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & \hline 35 \\ & (20) \\ & \hline \end{aligned}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1139 | 1069 | 1012 | 937 | 870 | 786 | 724 | 626 | 512 | 381 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 26 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 29 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 34 \\ & (19) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 47 \\ & (26) \\ & \hline \end{aligned}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{aligned} & 45 \\ & (25) \end{aligned}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1229 | 1171 | 1105 | 1049 | 980 | 913 | 838 | 775 | 679 | 516 |
|  |  |  |  | BHP | 0.28 | 0.30 | 0.30 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.34 | 0.33 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{aligned} & \hline 25 \\ & (14) \end{aligned}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \end{gathered}$ | $\begin{aligned} & 43 \\ & (24) \end{aligned}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  | High | Black | CFM | 1531 | 1460 | 1382 | 1301 | 1209 | 1114 | 1003 | 890 | 764 | 629 |
|  |  |  |  | BHP | 0.53 | 0.52 | 0.50 | 0.48 | 0.46 | 0.44 | 0.42 | 0.40 | 0.37 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | $\begin{gathered} 26 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 30 \\ & (17) \end{aligned}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | NA | NA |


| $\begin{aligned} & \hline \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 36060 | 25-55야 Low Stage, 25-55º High Stage | Low ${ }^{3}$ | Blue | CFM | 694 | 624 | 533 | 460 | 383 | 328 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.05 | 0.05 | 0.06 | 0.07 | 0.07 | 0.08 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 42 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  |  |  | BHP | 0.16 | 0.17 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} \hline 28 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  |  |  | BHP | 0.19 | 0.21 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{aligned} & \hline 32 \\ & (18) \end{aligned}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 36 \\ & (20) \\ & \hline \end{aligned}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ |
|  |  | High | Black | CFM | 1466 | 1423 | 1384 | 1343 | 1308 | 1263 | 1219 | 1183 | 1145 | 1106 |
|  |  |  |  | BHP | 0.30 | 0.31 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | $\begin{gathered} \hline 25 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 26 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{aligned} & 37 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & 39 \\ & (22) \\ & \hline \end{aligned}$ | $\begin{aligned} & 41 \\ & (23) \\ & \hline \end{aligned}$ |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNA | ATIC | ESSU | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 36090 | 35-65 F Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 882 | 737 | 665 | 608 | 542 | 496 | 437 | 395 | 339 | 288 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \hline 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  |  |  | BHP | 0.19 | 0.21 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} \hline 48 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ | $\begin{aligned} & 59 \\ & (33) \\ & \hline \end{aligned}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{aligned} & 64 \\ & (35) \end{aligned}$ | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1359 | 1311 | 1267 | 1224 | 1187 | 1140 | 1095 | 1058 | 1019 | 973 |
|  |  |  |  | BHP | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.31 | 0.33 | 0.34 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{aligned} & 39 \\ & \text { (22) } \end{aligned}$ | $\begin{aligned} & \hline 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 62 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA | NA |
|  |  | High | Black | CFM | 1466 | 1423 | 1384 | 1343 | 1308 | 1263 | 1219 | 1183 | 1145 | 1106 |
|  |  |  |  | BHP | 0.30 | 0.31 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \end{aligned}$ | $\begin{aligned} & \hline 52 \\ & (29) \\ & \hline \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{aligned} & 56 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 59 \\ & (33) \\ & \hline \end{aligned}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNA | TATIC | ESSU | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 42060 | 25-55야 Low Stage, 25-55ㅇF High Stage | Low ${ }^{3}$ | Blue | CFM | 694 | 624 | 533 | 460 | 383 | 328 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.05 | 0.05 | 0.06 | 0.07 | 0.07 | 0.08 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 42 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  |  |  | BHP | 0.13 | 0.14 | 0.15 | 0.15 | 0.17 | 0.18 | 0.18 | 0.20 | 0.21 | 0.22 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 27 \\ & (15) \end{aligned}$ | $\begin{aligned} & \hline 29 \\ & (16) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 32 \\ & (18) \end{aligned}$ | $\begin{aligned} & \hline 34 \\ & (19) \\ & \hline \end{aligned}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 38 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (27) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  |  |  | BHP | 0.16 | 0.17 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{aligned} & \hline 27 \\ & (15) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 28 \\ & (15) \end{aligned}$ | $\begin{gathered} 29 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 32 \\ & (18) \end{aligned}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{aligned} & 38 \\ & (21) \\ & \hline \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (24) \end{gathered}$ | 45 (25) | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ \text { (31) } \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  |  |  | BHP | 0.29 | 0.30 | 0.31 | 0.32 | 248.59 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{aligned} & 32 \\ & (18) \end{aligned}$ | $\begin{aligned} & \hline 33 \\ & (18) \\ & \hline \end{aligned}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 35 \\ & (20) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 36 \\ & (20) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  | High | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  |  |  | BHP | 0.41 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 28 \\ & (15) \end{aligned}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{aligned} & 29 \\ & (16) \end{aligned}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{aligned} & 32 \\ & (18) \end{aligned}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ |


| $\begin{aligned} & \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | HEATING RISE RANGE | MOTOR SPEED | WIRECOLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 42090 | 35-65야 Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 882 | 737 | 665 | 608 | 542 | 496 | 437 | 395 | 339 | 288 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  |  |  | BHP | 0.13 | 0.14 | 0.15 | 0.15 | 0.17 | 0.18 | 0.18 | 0.20 | 0.21 | 0.22 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \hline 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 51 \\ & (28) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 58 \\ & \text { (32) } \\ & \hline \end{aligned}$ | $\begin{aligned} & 62 \\ & (35) \\ & \hline \end{aligned}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 62 \\ (35) \end{gathered}$ | $\begin{gathered} 65 \\ (36) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1359 | 1311 | 1267 | 1224 | 1187 | 1140 | 1095 | 1058 | 1019 | 973 |
|  |  |  |  | BHP | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.31 | 0.33 | 0.34 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{aligned} & \hline 35 \\ & (19) \end{aligned}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} \hline 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{aligned} & 57 \\ & (32) \end{aligned}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{aligned} & 64 \\ & (36) \end{aligned}$ | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  |  |  | BHP | 0.29 | 0.30 | 0.31 | 0.32 | 248.59 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{aligned} & 47 \\ & (26) \end{aligned}$ | $\begin{gathered} \hline 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \end{aligned}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{aligned} & 61 \\ & (34) \end{aligned}$ |
|  |  | High | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  |  |  | BHP | 0.41 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & \hline 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{gathered} \hline 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 45 \\ & (25) \end{aligned}$ | $\begin{gathered} \hline 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 48 \\ & (27) \\ & \hline \end{aligned}$ | $\begin{aligned} & 49 \\ & (27) \end{aligned}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 51 \\ & (29) \end{aligned}$ |


| UNIT SIZE | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48090 | 35-65야 Low Stage, 35-65야 High Stage | Low ${ }^{3}$ | Blue | CFM | 903 | 820 | 749 | 702 | 645 | 581 | 534 | 468 | 432 | 382 |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.14 | 0.14 | 0.16 | 0.16 | 0.17 | 0.18 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{aligned} & \hline 43 \\ & (24) \\ & \hline \end{aligned}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{aligned} & 55 \\ & (31) \end{aligned}$ | $\begin{aligned} & 58 \\ & \text { (32) } \end{aligned}$ | $\begin{aligned} & 61 \\ & (34) \end{aligned}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1386 | 1336 | 1304 | 1259 | 1230 | 1186 | 1147 | 1102 | 1052 | 1022 |
|  |  |  |  | BHP | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.39 | 0.39 | 0.40 | 0.42 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{aligned} & \hline 39 \\ & (21) \end{aligned}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{aligned} & \hline 51 \\ & (28) \end{aligned}$ | $\begin{aligned} & 52 \\ & (29) \\ & \hline \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{aligned} & 59 \\ & (33) \end{aligned}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 45 \\ & (25) \\ & \hline \end{aligned}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{aligned} & 47 \\ & (26) \end{aligned}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ |
|  |  | High | Black | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 37 \\ & (21) \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & \hline 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & 39 \\ & \text { (22) } \end{aligned}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{aligned} & 43 \\ & (24) \\ & \hline \end{aligned}$ | $\begin{aligned} & 44 \\ & (25) \end{aligned}$ |


| $\begin{aligned} & \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48115 | 30-60F Low Stage, 30-60F High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 45 \\ & (25) \end{aligned}$ | $\begin{aligned} & 46 \\ & (26) \end{aligned}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{aligned} & 58 \\ & \text { (32) } \end{aligned}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 42 \\ & (24) \end{aligned}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{aligned} & \hline 46 \\ & (25) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 48 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 54 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{aligned} & 40 \\ & (22) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 51 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{aligned} & 56 \\ & (31) \end{aligned}$ | $\begin{gathered} 58 \\ \text { (32) } \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{aligned} & 60 \\ & (34) \end{aligned}$ | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{aligned} & 32 \\ & (18) \end{aligned}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (19) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 47 \\ & (26) \end{aligned}$ | $\begin{aligned} & 47 \\ & (26) \end{aligned}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | $\begin{aligned} & 53 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ \text { (31) } \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{aligned} & 31 \\ & (17) \end{aligned}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{aligned} & 32 \\ & (18) \end{aligned}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \\ & \hline \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ |


| $\begin{aligned} & \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48130 | 35-65 F Low Stage, 35-65${ }^{\circ}$ F High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{aligned} & 62 \\ & (34) \end{aligned}$ | $\begin{gathered} 65 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{aligned} & \hline 58 \\ & \text { (32) } \end{aligned}$ | $\begin{aligned} & \hline 61 \\ & (34) \\ & \hline \end{aligned}$ | $\begin{aligned} & 64 \\ & (35) \end{aligned}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{aligned} & 39 \\ & 22) \end{aligned}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 42 \\ & (24) \end{aligned}$ | $\begin{aligned} & 43 \\ & (24) \end{aligned}$ | $\begin{aligned} & 44 \\ & (25) \end{aligned}$ | $\begin{aligned} & 46 \\ & (25) \end{aligned}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 57 \\ & \text { (32) } \end{aligned}$ | $\begin{aligned} & 58 \\ & \text { (32) } \end{aligned}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 61 \\ & (34) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 62 \\ & (34) \end{aligned}$ | $\begin{aligned} & 64 \\ & \text { (35) } \end{aligned}$ | $\begin{gathered} 65 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{aligned} & 37 \\ & (21) \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{aligned} & 39 \\ & (22) \\ & \hline \end{aligned}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{aligned} & 56 \\ & (31) \end{aligned}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{aligned} & 63 \\ & \text { (35) } \end{aligned}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | $\begin{aligned} & \hline 35 \\ & (20) \end{aligned}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{aligned} & \hline 37 \\ & \text { (20) } \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{aligned} & 55 \\ & (31) \end{aligned}$ | $\begin{aligned} & 57 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{aligned} & 58 \\ & \text { (32) } \\ & \hline \end{aligned}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{aligned} & 63 \\ & \text { (35) } \end{aligned}$ |


| UNIT | HEATING RISE | MOTOR | WIRE |  |  |  |  | RNAL | ATIC | ESSU | (IN. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SIZE | RANGE | SPEED | COLOR |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60090 | 35-65야 Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 903 | 820 | 749 | 702 | 645 | 581 | 534 | 468 | 432 | 382 |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.14 | 0.14 | 0.16 | 0.16 | 0.17 | 0.18 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{aligned} & \hline 42 \\ & (23) \end{aligned}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{aligned} & 53 \\ & \text { (29) } \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{aligned} & 58 \\ & \text { (32) } \end{aligned}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1386 | 1336 | 1304 | 1259 | 1230 | 1186 | 1147 | 1102 | 1052 | 1022 |
|  |  |  |  | BHP | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.39 | 0.39 | 0.40 | 0.42 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{aligned} & 37 \\ & (21) \end{aligned}$ | $\begin{aligned} & \hline 39 \\ & (21) \end{aligned}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{aligned} & 43 \\ & (24) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \end{aligned}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{aligned} & \hline 37 \\ & (20) \end{aligned}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{aligned} & 44 \\ & (25) \end{aligned}$ |
|  |  | High | Black | CFM | 2020 | 1990 | 1956 | 1912 | 1872 | 1842 | 1802 | 1760 | 1719 | 1643 |
|  |  |  |  | BHP | 0.62 | 0.63 | 0.66 | 0.67 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 | 0.72 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |


| $\begin{aligned} & \text { UNIT } \\ & \text { SIZE } \end{aligned}$ | HEATING RISE RANGE | MOTOR SPEED | WIRECOLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60115 | 30-60F Low Stage 30-60F High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 45 \\ & (25) \end{aligned}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} \hline 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 51 \\ & (28) \end{aligned}$ | $\begin{aligned} & \hline 53 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 55 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{aligned} & 60 \\ & (33) \end{aligned}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 42 \\ & (24) \end{aligned}$ | $\begin{aligned} & 44 \\ & (24) \end{aligned}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{aligned} & \hline 48 \\ & (26) \end{aligned}$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{aligned} & 54 \\ & (30) \\ & \hline \end{aligned}$ | $\begin{gathered} 57 \\ (31) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 34 \\ & (19) \end{aligned}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{aligned} & \hline 41 \\ & (23) \\ & \hline \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \\ & \hline \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 51 \\ (29) \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} \hline 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{aligned} & 58 \\ & (32) \end{aligned}$ | $\begin{aligned} & 59 \\ & (33) \end{aligned}$ | $\begin{aligned} & 60 \\ & \text { (34) } \end{aligned}$ | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{aligned} & 33 \\ & (18) \end{aligned}$ | $\begin{gathered} 33 \\ (19) \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \end{gathered}$ | $\begin{aligned} & \hline 35 \\ & (19) \end{aligned}$ | $\begin{aligned} & 36 \\ & (20) \end{aligned}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 46 \\ & (26) \end{aligned}$ | $\begin{aligned} & 47 \\ & (26) \end{aligned}$ | $\begin{aligned} & 48 \\ & (27) \end{aligned}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{aligned} & 50 \\ & (28) \end{aligned}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \end{aligned}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{aligned} & 55 \\ & \text { (31) } \end{aligned}$ | $\begin{gathered} 57 \\ (31) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{aligned} & 30 \\ & (17) \end{aligned}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{aligned} & 32 \\ & (18) \end{aligned}$ | $\begin{array}{r} 33 \\ (18) \\ \hline \end{array}$ | $\begin{gathered} 33 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{aligned} & 35 \\ & (20) \end{aligned}$ | $\begin{aligned} & \hline 37 \\ & (21) \\ & \hline \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 45 \\ & (25) \end{aligned}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{aligned} & 49 \\ & (27) \end{aligned}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{aligned} & 52 \\ & (29) \\ & \hline \end{aligned}$ | $\begin{aligned} & 54 \\ & (30) \end{aligned}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ |

Table 13 - Dry Coil Air Delivery - Horizontal and Downflow Discharge - 208/230 VAC Single Phase Models (Cont)

| UNIT SIZE | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60130 | 35-65 F Low Stage, 35-65º High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{aligned} & 60 \\ & (33) \end{aligned}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 65 \\ (36) \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & \hline 48 \\ & (26) \\ & \hline \end{aligned}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & \hline 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & \hline 39 \\ & (21) \end{aligned}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{aligned} & 42 \\ & (24) \end{aligned}$ | $\begin{gathered} 43 \\ \text { (24) } \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{aligned} & 58 \\ & (32) \\ & \hline \end{aligned}$ | $\begin{aligned} & 59 \\ & (33) \\ & \hline \end{aligned}$ | $\begin{aligned} & 61 \\ & (34) \end{aligned}$ | $\begin{aligned} & \hline 62 \\ & (34) \end{aligned}$ | $\begin{aligned} & 64 \\ & \text { (35) } \end{aligned}$ | $\begin{gathered} 65 \\ (36) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{aligned} & 35 \\ & (19) \end{aligned}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 51 \\ & (28) \\ & \hline \end{aligned}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{array}{r} 54 \\ (30) \\ \hline \end{array}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ \text { (32) } \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | $\begin{aligned} & 35 \\ & (20) \end{aligned}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{aligned} & 38 \\ & (21) \end{aligned}$ | $\begin{aligned} & 40 \\ & (22) \end{aligned}$ | $\begin{aligned} & 42 \\ & (23) \end{aligned}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ \text { (29) } \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{aligned} & 55 \\ & \text { (31) } \end{aligned}$ | $\begin{aligned} & 57 \\ & \text { (31) } \end{aligned}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ |

Notes:
${ }^{1}$ Factory-shipped low stage cooling speed
${ }^{2}$ Factory-shipped high stage cooling speed
${ }^{3}$ Factory-shipped low stage gas heating speed
"NA" = Not allowed for particular heating speed

| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 24040 | 15-45야 Low Stage, 20-50F High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 26 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 41 \\ (23) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 689 | 597 | 489 | 352 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.06 | 0.06 | 0.05 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 877 | 779 | 698 | 598 | 519 | 410 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.12 | 0.12 | 0.13 | 0.14 | 0.15 | 0.15 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} \hline 21 \\ (12) \end{gathered}$ | $\begin{gathered} 24 \\ (13) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} \hline 36 \\ (20) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 921 | 829 | 754 | 663 | 582 | 485 | 371 | --- | --- | --- |
|  |  |  |  | BHP | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 | 0.17 | 0.18 | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 20 \\ (11) \end{gathered}$ | $\begin{gathered} 23 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 25 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | High | Black | CFM | 1291 | 1206 | 1142 | 1081 | 1017 | 951 | 888 | 823 | 753 | 668 |
|  |  |  |  | BHP | 0.31 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{aligned} & 15 \\ & \text { (8) } \end{aligned}$ | $\begin{aligned} & 16 \\ & \text { (9) } \end{aligned}$ | $\begin{aligned} & 16 \\ & (9) \end{aligned}$ | $\begin{gathered} \hline 17 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 18 \\ (10) \end{gathered}$ | $\begin{gathered} 20 \\ (11) \end{gathered}$ | $\begin{gathered} 21 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 23 \\ (13) \end{gathered}$ | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 23 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 24060 | 25-55ºF Low Stage, 25-55야 High Stage | Low ${ }^{1}$ | Blue | CFM | 689 | 597 | 489 | 352 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.06 | 0.06 | 0.05 | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 777 | 692 | 583 | 465 | 318 | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.09 | 0.10 | 0.10 | 0.11 | 0.12 | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 921 | 829 | 754 | 663 | 582 | 485 | 371 | --- | --- | --- |
|  |  |  |  | BHP | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 | 0.17 | 0.18 | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1229 | 1171 | 1105 | 1049 | 980 | 913 | 838 | 775 | 679 | 516 |
|  |  |  |  | BHP | 0.28 | 0.30 | 0.30 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.34 | 0.33 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | NA | NA | NA |
|  |  | High | Black | CFM | 1291 | 1206 | 1142 | 1081 | 1017 | 951 | 888 | 823 | 753 | 668 |
|  |  |  |  | BHP | 0.31 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRECOLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 30040 | 15-45야 Low Stage, 20-50F High Stage | Low ${ }^{3}$ | Blue | CFM | 714 | 525 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.08 | 0.07 | --- | --- | --- | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 26 \\ (15) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 831 | 765 | 670 | 586 | 466 | 299 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 23 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 25 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{array}{r} 38 \\ (21) \\ \hline \end{array}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 877 | 779 | 698 | 598 | 519 | 410 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.12 | 0.12 | 0.13 | 0.14 | 0.15 | 0.15 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 21 \\ (12) \end{gathered}$ | $\begin{gathered} 24 \\ (13) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1139 | 1069 | 1012 | 937 | 870 | 786 | 724 | 626 | 512 | 381 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{aligned} & 17 \\ & (9) \\ & \hline \end{aligned}$ | $\begin{gathered} 18 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 19 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 20 \\ (11) \end{gathered}$ | $\begin{gathered} 22 \\ (12) \end{gathered}$ | $\begin{gathered} 24 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 26 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 33 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | NA | NA |
|  |  | High | Black | CFM | 1531 | 1460 | 1382 | 1301 | 1209 | 1114 | 1003 | 890 | 764 | 629 |
|  |  |  |  | BHP | 0.53 | 0.52 | 0.50 | 0.48 | 0.46 | 0.44 | 0.42 | 0.40 | 0.37 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | $\begin{aligned} & 16 \\ & (9) \end{aligned}$ | $\begin{aligned} & 17 \\ & (9) \end{aligned}$ | $\begin{gathered} 19 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 20 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 21 \\ (12) \\ \hline \end{gathered}$ | $\begin{array}{r} 22 \\ (12) \\ \hline \end{array}$ | $\begin{gathered} 24 \\ (13) \end{gathered}$ | $\begin{gathered} 26 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 29 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 30060 | 25-55야 Low Stage, 25-55ºF High Stage | Low ${ }^{3}$ | Blue | CFM | 777 | 692 | 583 | 465 | 318 | --- | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.09 | 0.10 | 0.10 | 0.11 | 0.12 | --- | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 49 \\ (27) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 831 | 765 | 670 | 586 | 466 | 299 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.11 | 0.12 | 0.12 | 0.13 | 0.13 | 0.14 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1139 | 1069 | 1012 | 937 | 870 | 786 | 724 | 626 | 512 | 381 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ \text { (24) } \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1229 | 1171 | 1105 | 1049 | 980 | 913 | 838 | 775 | 679 | 516 |
|  |  |  |  | BHP | 0.28 | 0.30 | 0.30 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.34 | 0.33 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} \hline 27 \\ (15) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} \hline 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  | High | Black | CFM | 1531 | 1460 | 1382 | 1301 | 1209 | 1114 | 1003 | 890 | 764 | 629 |
|  |  |  |  | BHP | 0.53 | 0.52 | 0.50 | 0.48 | 0.46 | 0.44 | 0.42 | 0.40 | 0.37 | 0.35 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | NA | NA |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 36060 | 25-55야 Low Stage, 25-55º High Stage | Low ${ }^{3}$ | Blue | CFM | 694 | 624 | 533 | 460 | 383 | 328 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.05 | 0.05 | 0.06 | 0.07 | 0.07 | 0.08 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 48 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  |  |  | BHP | 0.16 | 0.17 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ \text { (22) } \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  |  |  | BHP | 0.19 | 0.21 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 29 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} \hline 32 \\ (18) \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ |
|  |  | High | Black | CFM | 1466 | 1423 | 1384 | 1343 | 1308 | 1263 | 1219 | 1183 | 1145 | 1106 |
|  |  |  |  | BHP | 0.30 | 0.31 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | $\begin{gathered} \hline 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (14) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 36090 | 35-65야 Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 1097 | 971 | 823 | 747 | 669 | 636 | 558 | 513 | 456 | 412 |
|  |  |  |  | BHP | 0.12 | 0.11 | 0.10 | 0.11 | 0.12 | 0.13 | 0.13 | 0.14 | 0.15 | 0.16 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  |  |  | BHP | 0.10 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.14 | 0.15 | 0.16 | 0.17 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 62 \\ (34) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  |  |  | BHP | 0.19 | 0.21 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} \hline 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{4}$ | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  |  |  | BHP | 0.29 | 0.30 | 0.31 | 0.32 | $\begin{gathered} 248 . \\ 59 \\ \hline \end{gathered}$ | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} \hline 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ |
|  |  | High | Black | CFM | 1466 | 1423 | 1384 | 1343 | 1308 | 1263 | 1219 | 1183 | 1145 | 1106 |
|  |  |  |  | BHP | 0.30 | 0.31 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ \text { (27) } \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 42060 | 25-55야 Low Stage, 25-55º High Stage | Low ${ }^{3}$ | Blue | CFM | 694 | 624 | 533 | 460 | 383 | 328 | --- | --- | --- | --- |
|  |  |  |  | BHP | 0.05 | 0.05 | 0.06 | 0.07 | 0.07 | 0.08 | --- | --- | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  |  |  | BHP | 0.13 | 0.14 | 0.15 | 0.15 | 0.17 | 0.18 | 0.18 | 0.20 | 0.21 | 0.22 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 47 \\ (26) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  |  |  | BHP | 0.16 | 0.17 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 26 \\ (14) \end{gathered}$ | $\begin{gathered} \hline 27 \\ (15) \end{gathered}$ | $\begin{gathered} \hline 28 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (16) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ \text { (22) } \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  |  |  | BHP | 0.29 | 0.30 | 0.31 | 0.32 | $\begin{gathered} 248 . \\ 59 \end{gathered}$ | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | $\begin{gathered} 25 \\ (14) \end{gathered}$ | $\begin{gathered} 26 \\ (15) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} \hline 34 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  | High | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  |  |  | BHP | 0.41 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 27 \\ (15) \end{gathered}$ | $\begin{gathered} 28 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 42090 | 35-65야 Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 1097 | 971 | 823 | 747 | 669 | 636 | 558 | 513 | 456 | 412 |
|  |  |  |  | BHP | 0.12 | 0.11 | 0.10 | 0.11 | 0.12 | 0.13 | 0.13 | 0.14 | 0.15 | 0.16 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  |  |  | BHP | 0.13 | 0.14 | 0.15 | 0.15 | 0.17 | 0.18 | 0.18 | 0.20 | 0.21 | 0.22 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} \hline 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \\ \hline \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium | Red | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  |  |  | BHP | 0.19 | 0.21 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  |  |  | BHP | 0.29 | 0.30 | 0.31 | 0.32 | $\begin{gathered} 248 . \\ 59 \end{gathered}$ | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  |  |  | BHP | 0.41 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (24) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48090 | 35-65야 Low Stage, 35-65야 High Stage | Low ${ }^{3}$ | Blue | CFM | 1067 | 904 | 703 | 587 | 501 | 449 | 380 | 340 | --- | --- |
|  |  |  |  | BHP | 0.12 | 0.10 | 0.09 | 0.09 | 0.09 | 0.10 | 0.11 | 0.12 | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{array}{r} 35 \\ (19) \\ \hline \end{array}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{array}{r} 35 \\ (19) \\ \hline \end{array}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 57 \\ (31) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ |
|  |  | High | Black | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48115 | 30-60F Low Stage, 30-60F High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} \hline 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} \hline 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 35 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48130 | 35-65야 Low Stage, 35-65야 High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 62 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 65(3 \\ 6) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | BHP | 0.56 | 0.57 | 0.60 | 0.59 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.67 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60090 | 35-65야 Low Stage, 35-65 F High Stage | Low ${ }^{3}$ | Blue | CFM | 1067 | 904 | 703 | 587 | 501 | 449 | 380 | 340 | --- | --- |
|  |  |  |  | BHP | 0.12 | 0.10 | 0.09 | 0.09 | 0.09 | 0.10 | 0.11 | 0.12 | --- | --- |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{1}$ | Pink | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 44 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{4}$ | Red | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ |
|  |  | High | Black | CFM | 2020 | 1990 | 1956 | 1912 | 1872 | 1842 | 1802 | 1760 | 1719 | 1643 |
|  |  |  |  | BHP | 0.62 | 0.63 | 0.66 | 0.67 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 | 0.72 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | $\begin{gathered} 35 \\ (20) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60115 | 30-60F Low Stage, 30-60F High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 57 \\ \text { (32) } \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 56 \\ \text { (31) } \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} \hline 31 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 30 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ |

Table 14 - Dry Coil Air Delivery* - Horizontal and Downflow Discharge - 208/230 VAC 3-Phase Models (Cont)

| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60130 | 35-65야 Low Stage, 35-65º High Stage | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | BHP | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1340 | 1299 | 1240 | 1191 | 1139 | 1091 | 1050 | 1001 | 952 | 895 |
|  |  |  |  | BHP | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} \hline 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA | NA |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | BHP | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.55 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 62 \\ (35) \end{gathered}$ | $\begin{gathered} \hline 64 \\ (35) \end{gathered}$ | $\begin{gathered} 65 \\ (36) \end{gathered}$ | NA | NA | NA |
|  |  | Med-High ${ }^{2}$ | Orange | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | BHP | 0.50 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 | 0.64 | 0.63 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ \text { (31) } \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ |
|  |  | High ${ }^{4}$ | Black | CFM | 1934 | 1900 | 1855 | 1815 | 1778 | 1737 | 1695 | 1656 | 1606 | 1528 |
|  |  |  |  | BHP | 0.59 | 0.61 | 0.62 | 0.64 | 0.65 | 0.67 | 0.68 | 0.70 | 0.70 | 0.68 |
|  |  |  |  | Low Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  |  |  | High Stage Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ \text { (31) } \end{gathered}$ | $\begin{gathered} 57 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ |

[^1][^2]| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 36060 | 25-55*F |  | Blue | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  | Low ${ }^{1}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{aligned} & 51 \\ & (29) \end{aligned}$ | $\begin{gathered} 55 \\ (30) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA |
|  |  |  | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  | Med-Low |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA | NA | NA | NA |
|  |  |  | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  | Medium ${ }^{3}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA |
|  |  |  | Orange | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  | Med-High ${ }^{2}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ |
|  |  |  | Black | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  | High |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | $\begin{gathered} 32 \\ (18) \end{gathered}$ | $\begin{gathered} 33 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
| 36090 | 35-65 ${ }^{\circ} \mathrm{F}$ | Low ${ }^{1}$ | Blue | CFM | 934 | 864 | 810 | 745 | 698 | 649 | 571 | 525 | 486 | 428 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  | Pink | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  | Med-Low |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  | Red | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  | Medium |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} \hline 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  |  | Orange | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  | Med-High ${ }^{2}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{array}{r} 57 \\ (32) \\ \hline \end{array}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  | Black | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  | High ${ }^{3}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \\ \hline \end{gathered}$ | $\begin{array}{r} 60 \\ (33) \\ \hline \end{array}$ | $\begin{gathered} 62 \\ (35) \end{gathered}$ |
| 42060 | 25-55 ${ }^{\circ} \mathrm{F}$ |  | Blue | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  | Low ${ }^{1}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA | NA | NA | NA |
|  |  |  | Pink | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  | Med-Low |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | NA |
|  |  |  | Red | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  | Medium ${ }^{3}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{array}{r} 48 \\ (26) \end{array}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ |
|  |  |  | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  | Med-High ${ }^{2}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 31 \\ (17) \end{gathered}$ | 31 <br> (17) | 32 <br> (18) | $\begin{gathered} 33 \\ (19) \end{gathered}$ | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  |  | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  | High |  | Heat Rise of $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 27 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 28 \\ (16) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 29 \\ (16) \end{gathered}$ | $\begin{gathered} 30 \\ (17) \\ \hline \end{gathered}$ | 31 <br> (17) | $\begin{gathered} \hline 32 \\ (18) \\ \hline \end{gathered}$ | 32(18) | $\begin{gathered} 33 \\ (18) \end{gathered}$ | $\begin{gathered} 34 \\ (19) \end{gathered}$ |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | WIRE COLOR |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 42090 | 35-65*F |  | Blue | CFM | 1076 | 1026 | 972 | 918 | 872 | 827 | 771 | 714 | 666 | 611 |
|  |  | Low ${ }^{1}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ <br> ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  | Pink | CFM | 1213 | 1169 | 1110 | 1065 | 1016 | 964 | 923 | 878 | 820 | 777 |
|  |  | Med-Low |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA | NA |
|  |  |  | Red | CFM | 1251 | 1198 | 1149 | 1104 | 1066 | 1017 | 970 | 932 | 892 | 839 |
|  |  | Medium |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \\ \hline \end{gathered}$ | $\begin{array}{r} 59 \\ (33) \\ \hline \end{array}$ | $\begin{gathered} 62 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  | Orange | CFM | 1451 | 1415 | 1372 | 1327 | 1287 | 1249 | 1212 | 1168 | 1130 | 1094 |
|  |  | Med-High ${ }^{2}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 62 \\ (35) \end{gathered}$ |
|  |  | High ${ }^{3}$ | Black | CFM | 1633 | 1590 | 1552 | 1518 | 1483 | 1444 | 1406 | 1372 | 1340 | 1303 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 42 \\ (\mathrm{D}) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $44$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ |
| 48090 | 35-65F |  | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  | Low ${ }^{1}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  |  | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  | Med-Low ${ }^{3}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $49$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 63 \\ (35) \end{gathered}$ | NA |  |
|  |  |  | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  | Medium ${ }^{2}$ |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ |
|  |  |  | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  | Med-High |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{aligned} & 41 \\ & (23) \end{aligned}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ |
|  |  | High | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ <br> ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ |  |
| 48115 | 30-60F | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 47 \\ \hline \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $48$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ |
|  |  | High ${ }^{3}$ | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 42 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{array}{r} 46 \\ (25) \\ \hline \end{array}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ |  |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | $\begin{aligned} & \text { WIRE } \\ & \text { COLOR } \end{aligned}$ |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 48130 | 35-65*F | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1686 | 1650 | 1617 | 1576 | 1544 | 1503 | 1468 | 1433 | 1393 | 1356 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \\ \hline \end{gathered}$ | $\begin{gathered} 62 \\ (35) \\ \hline \end{gathered}$ | $\begin{gathered} 64 \\ (36) \\ \hline \end{gathered}$ | NA | NA | NA | NA |
|  |  | Med-High | Orange | CFM | 1854 | 1837 | 1781 | 1784 | 1720 | 1698 | 1655 | 1625 | 1578 | 1532 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 57 \\ (32) \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 59 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} \hline 63 \\ (35) \\ \hline \end{gathered}$ |
|  |  | High ${ }^{3}$ | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ |  |
| 60090 | 35-65*F | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 54 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{array}{r} 58 \\ (32) \\ \hline \end{array}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{gathered} 64 \\ (35) \end{gathered}$ | NA | NA | NA | NA | NA |
|  |  | Med-Low ${ }^{3}$ | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 53 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{array}{r} 57 \\ (32) \\ \hline \end{array}$ | $\begin{array}{r} 60 \\ (33) \\ \hline \end{array}$ | $\begin{gathered} 63 \\ (35) \\ \hline \end{gathered}$ | NA |  |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 36 \\ (20) \end{gathered}$ | $\begin{gathered} \hline 37 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (21) \end{gathered}$ | $\begin{gathered} 39 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ |
|  |  | Med-High | Orange | CFM | 2020 | 1990 | 1956 | 1912 | 1872 | 1842 | 1802 | 1760 | 1719 | 1643 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | NA | NA | $\begin{gathered} 35 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 39 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} 40 \\ (22) \\ \hline \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ |
|  |  | High | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | $\begin{gathered} 35 \\ (19) \end{gathered}$ | $\begin{gathered} 36 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 37 \\ (20) \end{gathered}$ | $\begin{gathered} 38 \\ (21) \\ \hline \end{gathered}$ |  |
| 60115 | 30-60F | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 60 \\ (33) \\ \hline \end{gathered}$ | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (31) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ |
|  |  | Med-High | Orange | CFM | 2020 | 1990 | 1956 | 1912 | 1872 | 1842 | 1802 | 1760 | 1719 | 1643 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 43 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 44 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ |
|  |  | High ${ }^{3}$ | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise of $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 40 \\ \text { (22) } \end{gathered}$ | $\begin{gathered} 41 \\ (23) \end{gathered}$ | $\begin{gathered} 42 \\ (23) \end{gathered}$ | $\begin{gathered} 43 \\ \text { (24) } \end{gathered}$ | $\begin{gathered} 44 \\ (24) \end{gathered}$ | $\begin{gathered} 44 \\ (25) \end{gathered}$ | $\begin{gathered} 46 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ |  |


| UNIT | HEATING RISE RANGE | MOTOR SPEED | $\begin{aligned} & \text { WIRE } \\ & \text { COLOR } \end{aligned}$ |  | EXTERNAL STATIC PRESSURE (IN. W.C.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1 |
| 60130 | 35-65F | Low ${ }^{1}$ | Blue | CFM | 1271 | 1229 | 1177 | 1121 | 1066 | 1027 | 974 | 942 | 887 | 839 |
|  |  |  |  | Heat Rise ${ }^{\circ}{ }^{\circ}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Med-Low | Pink | CFM | 1445 | 1389 | 1341 | 1281 | 1236 | 1189 | 1139 | 1072 | 1027 |  |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  | Medium ${ }^{2}$ | Red | CFM | 1878 | 1844 | 1805 | 1762 | 1731 | 1693 | 1655 | 1616 | 1570 | 1532 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 51 \\ (28) \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \end{gathered}$ | $\begin{gathered} 55 \\ (30) \end{gathered}$ | $\begin{gathered} 56 \\ (31) \end{gathered}$ | $\begin{gathered} 57 \\ \text { (32) } \end{gathered}$ | $\begin{gathered} 58 \\ (32) \end{gathered}$ | $\begin{gathered} 60 \\ (33) \end{gathered}$ | $\begin{gathered} 61 \\ (34) \end{gathered}$ | $\begin{aligned} & 63 \\ & \text { (35) } \end{aligned}$ |
|  |  | Med-High | Orange | CFM | 2020 | 1990 | 1956 | 1912 | 1872 | 1842 | 1802 | 1760 | 1719 | 1643 |
|  |  |  |  | Heat Rise ${ }^{\circ} \mathrm{F}$ ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} 48 \\ (26) \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \end{gathered}$ | $\begin{gathered} 51 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \end{gathered}$ | $\begin{gathered} 53 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 55 \\ (30) \\ \hline \end{gathered}$ | $\begin{gathered} 56 \\ (31) \\ \hline \end{gathered}$ | $\begin{gathered} 59 \\ (33) \\ \hline \end{gathered}$ |
|  |  | High ${ }^{3}$ | Black | CFM | 2131 | 2088 | 2065 | 2013 | 1982 | 1941 | 1888 | 1860 | 1785 |  |
|  |  |  |  | Heat Rise OF $\left({ }^{\circ} \mathrm{C}\right)$ | $\begin{gathered} 45 \\ (25) \\ \hline \end{gathered}$ | $\begin{gathered} 46 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 47 \\ (26) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (27) \\ \hline \end{gathered}$ | $\begin{gathered} 49 \\ (27) \end{gathered}$ | $\begin{gathered} 50 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 51 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 52 \\ (29) \\ \hline \end{gathered}$ | $\begin{gathered} 54 \\ (30) \\ \hline \end{gathered}$ |  |

[^3]Table 16 - Wet Coil Pressure Drop (IN. W.C.)




| OిNN | 1 | ' | $\stackrel{10}{0}$ |
| :---: | :---: | :---: | :---: |
| $\frac{\mathrm{O}}{\mathrm{~N}}$ | ' | ' | $\frac{\pi}{0}$ |
| oid | ' | ' | $\stackrel{m}{\square}$ |
| O- | ' | ' | $\underset{\sim}{\square}$ |
| O | ' | $\stackrel{N}{O}$ | $\bigcirc$ |
| $\stackrel{\otimes}{\underset{\sim}{\circ}}$ | ' | $\underset{0}{\mathrm{~F}}$ | $\stackrel{\circ}{\circ}$ |



| FILTER SIZE IN. (MM) | $\begin{aligned} & \text { COOLING } \\ & \text { TONS } \end{aligned}$ | STANDARD CF |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 600 | 700 | 800 | 900 | 1000 | 1100 | 1200 | 1300 | 1400 |
| $\begin{gathered} 600-1400 \text { CFM } \\ 12 \times 20 \times 1+12 \times 20 \times 1 \\ (305 \times 508 \times 25+305 \times 508 \times 25) \end{gathered}$ | $\begin{aligned} & 2.0, \\ & 2.5 \end{aligned}$ | 0.03 | 0.05 | 0.06 | 0.08 | 0.10 | 0.11 | 0.13 | 0.14 | 0.16 |
| $1200-1800$ CFM $16 \times 24 \times 1+14 \times 24 \times 1$ $(406 \times 610 \times 25+356 \times 610 \times 25)$ | $\begin{gathered} 3.0, \\ 3.5 \end{gathered}$ | - | - | - | - | - | - | 0.07 | 0.08 | 0.09 |
| $\begin{gathered} 1500-2200 \text { CFM } \\ 16 \times 24 \times 1+18 \times 24 \times 1 \\ (406 \times 610 \times 25+457 \times 610 \times 25) \end{gathered}$ | $\begin{aligned} & \text { 4.0, } \\ & 5.0 \end{aligned}$ | - | - | - | - | - | - | - | - | - |

## MAINTENANCE

To ensure continuing high performance and to minimize the possibility of premature equipment failure, periodic maintenance must be performed on this equipment. This unit should be inspected at least once each year by a qualified service person. To troubleshoot unit, refer to Table 19-21, Troubleshooting Chart.
NOTE TO EQUIPMENT OWNER: Consult your local dealer about the availability of a maintenance contract.

## 4 WARNING

## PERSONAL INJURY AND UNIT DAMAGE HAZARD

Failure to follow this warning could result in personal injury or death and unit component damage.
The ability to properly perform maintenance on this equipment requires certain expertise, mechanical skills, tools and equipment. If you do not possess these, do not attempt to perform any maintenance on this equipment, other than those procedures recommended in the Owner's Manual.

## 4 WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow these warnings could result in personal injury or death:

1. Turn off electrical power to the unit and install lock out tag before performing any maintenance or service on this unit.
2. Use extreme caution when removing panels and parts.
3. Never place anything combustible either on or in contact with the unit.

## 4 CAUTION

## UNIT OPERATION HAZARD

Failure to follow this caution may result in improper operation.
Errors made when reconnecting wires may cause improper and dangerous operation. Label all wires prior to disconnecting when servicing.

## 1 CAUTION

## ENVIRONMENTAL HAZARD

Failure to follow this caution may result in environmental pollution.
Remove and re-cycle all components or materials (i.e. oil, refrigerant, etc) before unit final disposal.

The minimum maintenance requirements for this equipment are as follows:

1. Inspect air filter(s) each month. Clean or replace when necessary.
2. Inspect indoor coil, drain pan, and condensate drain each cooling season for cleanliness. Clean when necessary.
3. Inspect blower motor and wheel for cleanliness at the beginning of each heating and cooling season. Clean when necessary. For first heating and cooling season, inspect blower wheel bi-monthly to determine proper cleaning frequency.
4. Check electrical connections for tightness and controls for proper operation each heating and cooling season. Service when necessary.
5. Ensure electric wires are not in contact with refrigerant tubing or sharp metal edges.
6. Check and inspect heating section before each heating season. Clean and adjust when necessary.
7. Check flue hood and remove any obstructions, if necessary.

## Air Filter

IMPORTANT: Never operate the unit without a suitable air filter in the return-air duct system. Always replace the filter with the same dimensional size and type as originally installed. See Table 1 for recommended filter sizes.
Inspect air filter(s) at least once each month and replace (throwaway-type) or clean (cleanable-type) at least twice during each cooling season and twice during the heating season, or whenever the filter becomes clogged with dust and lint.

## Indoor Blower and Motor

NOTE: All motors are pre-lubricated. Do not attempt to lubricate these motors.
For longer life, operating economy, and continuing efficiency, clean accumulated dirt and grease from the blower wheel and motor annually.

## WARNING

## ELECTRICAL SHOCK HAZARD

Failure to follow this warning could result in personal injury or death.

Disconnect and tag electrical power to the unit before cleaning the blower motor and wheel.

To clean the blower motor and wheel:

1. Remove and disassemble blower assembly as follows:
a. Remove blower access panel (see Fig. 24).
b. Disconnect 5 pin plug and 4 pin plug from indoor blower motor. Remove capacitor if required.
c. On all units remove blower assembly from unit. Remove screws securing blower to blower partition and slide assembly out. Be careful not to tear insulation in blower compartment.
d. Ensure proper reassembly by marking blower wheel and motor in relation to blower housing before disassembly.
e. Loosen setscrew(s) that secures wheel to motor shaft, remove screws that secure motor mount brackets to housing, and slide motor and motor mount out of housing.
2. Remove and clean blower wheel as follows:
a. Ensure proper reassembly by marking wheel orientation.
b. Lift wheel from housing. When handling and/or cleaning blower wheel, be sure not to disturb balance weights (clips) on blower wheel vanes.
c. Remove caked-on dirt from wheel and housing with a brush. Remove lint and/or dirt accumulations from wheel and housing with vacuum cleaner, using soft brush attachment. Remove grease and oil with mild solvent.
d. Reassemble wheel into housing.
e. Reassemble motor into housing. Be sure setscrews are tightened on motor shaft flats and not on round part of shaft. Reinstall blower into unit. Reinstall capacitor.
f. Connect 5 pin plug and 4 pin plug to indoor blower motor.
g. Reinstall blower access panel (see Fig. 24).
3. Restore electrical power to unit. Start unit and check for proper blower rotation and motor speeds during heating and cooling cycles.

## Induced Draft (combustion air) Blower Assembly

The induced-draft blower assembly consists of the inducer motor, the blower housing, and the induced-draft blower wheel.
Clean periodically to assure proper airflow and heating efficiency. Inspect blower wheel every fall and periodically during the heating season. For the first heating season, inspect blower wheel bimonthly to determine proper cleaning frequency.
To inspect blower wheel, remove draft hood assembly. Shine a flashlight into opening to inspect wheel. If cleaning is required, remove induced-draft blower assembly as follows:

1. Remove control access panel (See Fig. 24).
2. Remove the 5 screws that attach induced-draft blower assembly to the flue collector box cover.
3. Slide the assembly out of the unit. (See Fig. 26). Clean the blower wheel. If additional cleaning is required, continue with Steps 4 and 5.
4. To remove blower wheel, remove 2 setscrews.
5. To remove inducer motor, remove screws that hold the inducer motor to the blower housing.
6. To reinstall, reverse the procedure outlined above.

## Flue Gas Passageways1

To inspect the flue collector box and upper areas of the heat exchanger:

1. Remove the induced draft blower assembly according to directions in the Induced Draft Blower Assembly section.
2. Remove the 11 screws holding the flue collector box cover (See Fig. 23) to the heat exchanger assembly. Inspect the heat exchangers.
3. Clean all surfaces, as required, using a wire brush.

## Limit Switch

Remove blower access panel (see Fig. 24). Limit switch(es) are located on the fan partition.

## Burner Ignition

Unit is equipped with a direct spark ignition 100 percent lockout system. Ignition module (IGC) is located in the control box (See Fig. 23). Module contains a self-diagnostic LED. During servicing, refer to label diagram or Table 8 in these instructions for LED interpretation.
If lockout occurs, unit may be reset by either momentarily interrupting power supply to unit or by turning selector switch to OFF position at the thermostat.

## Main Burners

At the beginning of each heating season, inspect for deterioration or blockage due to corrosion or other causes. Observe the main burner flames and adjust, if necessary.

## Removal of Gas Train

To remove the gas train for servicing:

1. Shut off main gas valve.
2. Shut off power to unit and install lockout tag.
3. Remove control access panel (See Fig. 24).
4. Disconnect gas piping at unit gas valve.
5. Remove fan partition mounting bracket ( 2 screws located on the left side of control compartment on the fan partition panel). Slide bracket forward, bottom first, to remove. (See Fig. 23.)
6. Remove wires connected to gas valve. Mark each wire.
7. Remove the mounting screw that attaches the burner rack to the unit base (See Fig. 23).
8. Partially slide the burner rack out of the unit (see Fig. 23 and 26). Remove ignitor and sensor wires at the burner assembly. Remove wires to rollout switch.
9. Slide the burner rack out of the unit (See Fig. 23 and 26).
10. To reinstall, reverse the procedure outlined above.
11. Check all connections for leaks.


## FIRE, EXPLOSION HAZARD

Failure to follow this warning could result in personal injury, death or property damage.
Do not purge gas supply into the combustion chamber. Do not use a match or other open flame to check for gas leaks. Use a commercially available soap solution made specifically for the detection of leaks to check all connections. A fire or explosion may result causing property damage, personal injury or loss of life.

## Outdoor Coil, Indoor Coil, and Condensate Drain Pan

Inspect the condenser coil, evaporator coil, and condensate drain pan at least once each year.
The coils are easily cleaned when dry; therefore, inspect and clean the coils either before or after each cooling season. Remove all obstructions, including weeds and shrubs, that interfere with the airflow through the condenser coil.
Straighten bent fins with a fin comb. If coated with dirt or lint, clean the coils with a vacuum cleaner, using the soft brush attachment. Be careful not to bend the fins. If coated with oil or grease, clean the coils with a mild detergent and water solution. Rinse coils with clear water, using a garden hose. Be careful not to splash water on motors, insulation, wiring, or air filter(s). For best results, spray condenser coil fins from inside to outside the unit. On units with an outer and inner condenser coil, be sure to clean between the coils. Be sure to flush all dirt and debris from the unit base.
Inspect the drain pan and condensate drain line when inspecting the coils. Clean the drain pan and condensate drain by removing all foreign matter from the pan. Flush the pan and drain trough with clear water. Do not splash water on the insulation, motor, wiring, or air filter(s). If the drain trough is restricted, clear it with a "plumbers snake" or similar probe device.


Fig. 23 - Blower Housing and Flue Collector Box


Fig. 24 - Unit Access Panels


C99085
Fig. 25 - Removal of Motor and Blower Wheel


Fig. 26 - Burner Rack Removed

## Outdoor Fan

## 4 CAUTION

## UNIT OPERATION HAZARD

Failure to follow this caution may result in damage to unit components.

Keep the condenser fan free from all obstructions to ensure proper cooling operation. Never place articles on top of the unit.

1. Remove 6 screws holding outdoor grille and motor to top cover.
2. Turn motor/grille assembly upside down on top cover to expose fan blade.
3. Inspect the fan blades for cracks or bends.
4. If fan needs to be removed, loosen setscrew and slide fan off motor shaft.
5. When replacing fan blade, position blade as shown in Fig. 27.
6. Ensure that setscrew engages the flat area on the motor shaft when tightening.
7. Replace grille.

## Electrical Controls and Wiring

Inspect and check the electrical controls and wiring annually. Be sure to turn off the electrical power to the unit.
Remove access panels (see Fig. 24) to locate all the electrical controls and wiring. Check all electrical connections for tightness. Tighten all screw connections. If any smoky or burned connections are noticed, disassemble the connection, clean all the parts, re-strip the wire end and reassemble the connection properly and securely.
After inspecting the electrical controls and wiring, replace all the panels. Start the unit, and observe at least one complete cooling cycle to ensure proper operation. If discrepancies are observed in operating cycle, or if a suspected malfunction has occurred, check each electrical component with the proper electrical instrumentation. Refer to the unit wiring label when making these checks.


MAX DISTANCE BETWEEN TOP OF FAN GRILLE AND BOTTOM OF FAN BLADE

| SIZE |  | "A" |
| :---: | :---: | :---: |
|  | IN. | MM |
| 24 | 6.3 | 160 |
| 30 | 6.3 | 160 |
| 36 | 7.6 | 193 |
| 42 | 7.6 | 193 |
| 48 | 7.6 | 193 |
| 60 | 7.6 | 193 |

Fig. 27 - Fan Blade Position

## Refrigerant Circuit

Annually inspect all refrigerant tubing connections and the unit base for oil accumulations.

## 4 WARNING

## EXPLOSION, SAFETY AND ENVIRONMENTAL HAZARD

Failure to follow this warning could result in personal injury, death or property damage.
System under pressure. Relieve pressure and recover all refrigerant before system repair or final unit disposal. Use all service ports and open all flow-control devices, including solenoid valves.

If low cooling performance is suspected, leak-test all refrigerant tubing using an electronic leak-detector, halide torch, or liquid-soap solution. If a refrigerant leak is detected, refer to the Check for Refrigerant Leaks section.
If no refrigerant leaks are found and low cooling performance is suspected, refer to the Checking and Adjusting Refrigerant Charge section.

## Gas Input

The gas input does not require checking unless improper heating performance is suspected. If a problem exists, refer to the Start-Up section.

## Evaporator Airflow

The heating and/or cooling airflow does not require checking unless improper performance is suspected. If a problem exists, be sure that all supply- and return-air grilles are open and free from obstructions, and that the air filter is clean. When necessary, refer to the Indoor Airflow and Airflow Adjustments section to check the system airflow.

## Puron Items

## Metering Device (Thermostatic Expansion Valve)

This metering device is a hard shutoff, balance port TXV. The TXV maintains a constant superheat at the evaporator exit resulting in higher overall system efficiency.

## Pressure Switches

Pressure switches are protective devices wired into control circuit (low voltage). They shut off compressor if abnormally high or low pressures are present in the refrigeration circuit. These pressure switches are specifically designed to operate with Puron (R-410A) systems. R-22 pressure switches must not be used as replacements for the Puron (R-410A) system.

## Loss of Charge Switch

This switch is located on the liquid line and protects against low suction pressures caused by such events as loss of charge, low airflow across indoor coil, dirty filters, etc. It opens on a pressure drop at about 20 psig. If system pressure is above this, switch should be closed. To check switch:

1. Turn off all power to unit.
2. Disconnect leads on switch.
3. Apply ohm meter leads across switch. You should have continuity on a good switch.
NOTE: Because these switches are attached to refrigeration system under pressure, it is not advisable to remove this device for troubleshooting unless you are reasonably certain that a problem exists. If switch must be removed, remove and recover all system charge so that pressure gauges read 0 psig. Never open system without breaking vacuum with dry nitrogen.

## High-Pressure Switch

The high-pressure switch is located in the discharge line and protects against excessive condenser coil pressure. It opens at 650 psig.
High pressure may be caused by a dirty outdoor coil, failed fan motor, or outdoor air recirculation. To check switch:

1. Turn off all power to unit.
2. Disconnect leads on switch.
3. Apply ohm meter leads across switch. You should have continuity on a good switch.

## Copeland Scroll Compressor (Puron Refrigerant)

The compressor used in this product is specifically designed to operate with Puron (R-410A) refrigerant and cannot be interchanged.
The compressor is an electrical (as well as mechanical) device. Exercise extreme caution when working near compressors. Power should be shut off, if possible, for most troubleshooting techniques. Refrigerants present additional safety hazards.

## 4 WARNING

## FIRE/EXPLOSION HAZARD

Failure to follow this warning could result in personal injury or death and/or property damage.
Wear safety glasses and gloves when handling refrigerants. Keep torches and other ignition sources away from refrigerants and oils.

The scroll compressor pumps refrigerant throughout the system by the interaction of a stationary and an orbiting scroll. The scroll compressor has no dynamic suction or discharge valves, and it is more tolerant of stresses caused by debris, liquid slugging, and flooded starts. The compressor is equipped with a noise reducing shutdown device and an internal pressure relief port. The pressure relief port is a safety device, designed to protect against extreme high pressure. The relief port has an operating range between 550 ( 26.34 kPa ) and $625 \mathrm{psig}(29.93 \mathrm{kPa}$ ) differential pressure.


Failure to follow this warning could result in personal injury, death or equipment damage.
This system uses Puron (R-410A) refrigerant which has higher operating pressures than $\mathrm{R}-22$ and other refrigerants. No other refrigerant may be used in this system. Gauge set, hoses, and recovery system must be designed to handle Puron. If you are unsure, consult the equipment manufacturer.

## Refrigerant System

This information covers the refrigerant system including the compressor oil needed, servicing systems on roofs containing synthetic materials, the filter drier and refrigerant charging.

## Compressor Oil

The Copeland scroll compressor uses 3MAF POE oil. If additional oil is needed, use Uniqema RL32-3MAF. If this oil is not available, use Copeland Ultra 32 CC or Mobil Arctic EAL22 CC. This oil is extremely hygroscopic, meaning it absorbs water readily. POE oils can absorb 15 times as much water as other oils designed for HCFC and CFC refrigerants. Take all necessary precautions to avoid exposure of the oil to the atmosphere.

Servicing Systems on Roofs with Synthetic Materials
POE (polyolester) compressor lubricants are known to cause long term damage to some synthetic roofing materials.
Exposure, even if immediately cleaned up, may cause embrittlement (leading to cracking) to occur in one year or more. When performing any service that may risk exposure of compressor oil to the roof, take appropriate precautions to protect roofing. Procedures which risk oil leakage include, but are not limited to, compressor replacement, repairing refrigerant leaks, replacing refrigerant components such as filter drier, pressure switch, metering device, coil, accumulator, or reversing valve.

## Synthetic Roof Precautionary Procedure

1. Cover extended roof working area with an impermeable polyethylene (plastic) drip cloth or tarp. Cover an approximate $10 \times 10 \mathrm{ft}$. ( 3.1 m X 3.1 m ) area.
2. Cover area in front of the unit service panel with a terry cloth shop towel to absorb lubricant spills and prevent run-offs, and protect drop cloth from tears caused by tools or components.
3. Place terry cloth shop towel inside unit immediately under component(s) to be serviced and prevent lubricant run-offs through the louvered openings in the unit base.
4. Perform required service.
5. Remove and dispose of any oil contaminated material per local codes.

## Liquid Line Filter Drier

This filter drier is specifically designed to operate with Puron. Use only factory-authorized components. Filter drier must be replaced whenever the refrigerant system is opened. When removing a filter drier, use a tubing cutter to cut the drier from the system. Do not unsweat a filter drier from the system. Heat from unsweating will release moisture and contaminants from drier into system.

## Puron (R-410A) Refrigerant Charging

Refer to unit information plate and charging chart. Some R-410A refrigerant cylinders contain a dip tube to allow liquid refrigerant to flow from cylinder in upright position. For cylinders equipped with a dip tube, charge Puron units with cylinder in upright position and a commercial metering device in manifold hose. Charge refrigerant into suction-line.

## TROUBLESHOOTING

Use the Troubleshooting Guides (See Tables 19-21) if problems occur with these units.

## START-UP CHECKLIST

Use Start-Up checklist to ensure proper start-up procedures are followed.

## PURON® ${ }^{\circledR}$ (R-410A) QUICK REFERENCE GUIDE

- Puron refrigerant operates at 50-70 percent higher pressures than $\mathrm{R}-22$. Be sure that servicing equipment and replacement components are designed to operate with Puron
- Puron refrigerant cylinders are rose colored.
- Recovery cylinder service pressure rating must be 400 psig, DOT 4BA400 or DOT BW400.
- Puron systems should be charged with liquid refrigerant. Use a commercial type metering device in the manifold hose when charging into suction line with compressor operating
- Manifold sets should be minimum 700 psig high side and 180 psig low side with 550 psig low-side retard.
- Use hoses with minimum 700 psig service pressure rating.
- Leak detectors should be designed to detect HFC refrigerant.
- Puron, as with other HFCs, is only compatible with POE oils.
- Vacuum pumps will not remove moisture from oil.
- Do not use liquid-line filter driers with rated working pressures less than 600 psig .
- Do not leave Puron suction line filter driers in line longer than 72 hrs .
- Do not install a suction-line filter drier in liquid line.
- POE oils absorb moisture rapidly. Do not expose oil to atmosphere.
- POE oils may cause damage to certain plastics and roofing materials.
- Wrap all filter driers and service valves with wet cloth when brazing.
- A factory approved liquid-line filter drier is required on every unit.
- Do NOT use an R-22 TXV.
- Never open system to atmosphere while it is under a vacuum.
- When system must be opened for service, recover refrigerant, evacuate then break vacuum with dry nitrogen and replace filter driers. Evacuate to 500 microns prior to recharging.
- Do not vent Puron into the atmosphere.
- Observe all warnings, cautions, and bold text.
- All indoor coils must be installed with a hard shutoff Puron TXV metering device.

Table 19 - Troubleshooting Chart

| SYMPTOM | CAUSE | REMEDY |
| :---: | :---: | :---: |
| Compressor and condenser fan will not start. | Power failure | Call power company |
|  | Fuse blown or circuit breaker tripped | Replace fuse or reset circuit breaker |
|  | Defective contactor, transformer, or high-pressure, loss-of-charge or low-pressure switch | Replace component |
|  | Insufficient line voltage | Determine cause and correct |
|  | Incorrect or faulty wiring | Check wiring diagram and rewire correctly |
|  | Thermostat setting too high | Lower thermostat temperature setting below room temperature |
| Compressor will not start but condenser fan runs | Faulty wiring or loose connections in compressor circuit | Check wiring and repair or replace |
|  | Compressor motor burned out, seized, or internal overload open | Determine cause <br> Replace compressor |
|  | Defective run/start capacitor, overload, start relay | Determine cause and replace |
|  | One leg of 3-phase power dead | Replace fuse or reset circuit breaker Determine cause |
|  | Low input voltage | Determine cause and correct |
| Three-phase scroll compressor makes excessive noise, and there may be a low pressure differential. | Scroll compressor is rotating in the wrong direction | Correct the direction of rotation by reversing the 3-phase power leads to the unit. Shut down unit to allow pressures to equalize. |
| Compressor cycles (other than normally satisfying thermostat) | Refrigerant overcharge or undercharge | Recover refrigerant, evacuate system, and recharge to capacities shown on rating plate |
|  | Defective compressor | Replace and determine cause |
|  | Insufficient line voltage | Determine cause and correct |
|  | Blocked outdoor coil | Determine cause and correct |
|  | Defective run/start capacitor | Determine cause and replace |
|  | Faulty outdoor fan motor or capacitor | Replace |
|  | Restriction in refrigerant system | Locate restriction and remove |
| Compressor operates continuously | Dirty air filter | Replace filter |
|  | Unit undersized for load | Decrease load or increase unit size |
|  | Thermostat temperature set too low | Reset thermostat |
|  | Low refrigerant charge | Locate leak, repair, and recharge |
|  | Air in system | Recover refrigerant, evacuate system, and recharge |
|  | Outdoor coil dirty or restricted | Clean coil or remove restriction |
| Excessive head pressure | Dirty air filter | Replace filter |
|  | Dirty condenser coil | Clean coil |
|  | Refrigerant overcharged | Recover excess refrigerant |
|  | Air in system | Recover refrigerant, evacuate system, and recharge |
|  | Condenser air restricted or air short-cycling | Determine cause and correct |
| Head pressure too low | Low refrigerant charge | Check for leaks, repair, and recharge. |
|  | Restriction in liquid tube | Remove restriction |
| Excessive suction pressure | Refrigerant overcharged | Recover excess refrigerant |
| Suction pressure too low | Dirty air filter | Replace filter |
|  | Low refrigerant charge | Check for leaks, repair and recharge |
|  | Metering device or low side restricted | Remove source of restriction |
|  | Insufficient evaporator airflow | Increase air quantity Check filter-replace if necessary |
|  | Temperature too low in conditioned area | Reset thermostat |
|  | Outdoor ambient below $55^{\circ} \mathrm{F}\left(13^{\circ} \mathrm{C}\right)$ | Install low-ambient kit |
|  | Filter drier restricted | Replace filter |

Table 20 - Troubleshooting Guide-Heating

| SYMPTOM | CAUSE | REMEDY |
| :---: | :---: | :---: |
| Burners will not ignite | Water in gas line | Drain. Install drip leg. |
|  | No power to furnace | Check power supply fuses, wiring or circuit breaker. |
|  | No 24-v power supply to control circuit | Check transformer. <br> NOTE: Some transformers have internal over-current protection that requires a cool-down period to reset. |
|  | Mis-wired or loose connections | Check all wiring and wire nut connections |
|  | Misaligned spark electrodes | Check flame ignition and sense electrode positioning. Adjust as necessary. |
|  | No gas at main burners | 1. Check gas line for air. Purge as necessary. NOTE: After purging gas line of air, wait at least 5 minutes for any gas to dissipate before attempting to light unit. <br> 2. Check gas valve. |
| Inadequate heating | Dirty air filter | Clean or replace filter as necessary |
|  | Gas input to furnace too low | Check gas pressure at manifold match with that on unit nameplate |
|  | Unit undersized for application | Replace with proper unit or add additional unit |
|  | Restricted airflow | Clean or replace filter. Remove any restriction. |
|  | Limit switch cycles main burners | Check rotation of blower, temperature rise of unit. Adjust as necessary. |
| Poor flame characteristics | Incomplete combustion results in: Aldehyde odors, carbon monoxide, sooting flame, floating flame | 1. Tighten all screws around burner compartment <br> 2. Cracked heat exchanger. Replace. <br> 3. Unit over-fired. Reduce input (change orifices or adjust gas line or manifold pressure). <br> 4. Check burner alignment. <br> 5. Inspect heat exchanger for blockage. Clean as necessary. |

Table 21 - Troubleshooting Guide-LED Status Codes

| SYMPTOM |  | CAUSE |
| :--- | :--- | :--- |
| No Power or Hardware fail- <br> ure <br> (LED OFF) | Loss of power to control module (IGC)*. | REMEDY |

*WARNING $\widehat{\triangle}$ : If the IGC must be replaced, be sure to ground yourself to dissipate any electrical charge that my be present before handling new control board. The IGC is sensitive to static electricity and my be damaged if the necessary precautions are not taken.
IMPORTANT: Refer to Table 20-Troubleshooting Guide-Heating for additional troubleshooting analysis.
LEGEND
IGC-Integrated Gas Unit Controller
LED-Light-Emitting Diode

# START-UP CHECKLIST 

(Remove and Store in Job Files)

## I. PRELIMINARY INFORMATION

MODEL NO.: $\qquad$
SERIAL NO.: $\qquad$
DATE: $\qquad$
TECHNICIAN: $\qquad$
II. PRESTART-UP (Insert check mark in box as each item is completed)
( ) VERIFY THAT ALL PACKING MATERIALS HAVE BEEN REMOVED FROM UNIT
( ) REMOVE ALL SHIPPING HOLD DOWN BOLTS AND BRACKETS PER INSTALLATION INSTRUCTIONS
( ) CHECK ALL ELECTRICAL CONNECTIONS AND TERMINALS FOR TIGHTNESS
( ) CHECK GAS PIPING FOR LEAKS (WHERE APPLICABLE)
( ) CHECK THAT INDOOR (EVAPORATOR) AIR FILTER IS CLEAN AND IN PLACE
( ) VERIFY THAT UNIT INSTALLATION IS LEVEL
( ) CHECK FAN WHEEL, AND PROPELLER FOR LOCATION IN HOUSING/ORIFICE AND SETSCREW TIGHTNESS

## III. START-UP

ELECTRICAL
SUPPLY VOLTAGE $\qquad$ COMPRESSOR AMPS
INDOOR (EVAPORATOR) FAN AMPS $\qquad$
TEMPERATURES
OUTDOOR (CONDENSER) AIR TEMPERATURE $\qquad$ DB
RETURN-AIR TEMPERATURE $\qquad$ DB WB
COOLING SUPPLY AIR $\qquad$ DB $\qquad$ WB
GAS HEAT SUPPLY AIR PRESSURES
GAS INLET PRESSURE $\qquad$ IN. W.C.
GAS MANIFOLD PRESSURE (HIGH STAGE) $\qquad$ IN. W.C.
GAS MANIFOLD PRESSURE (LOW STAGE, 208/230 VAC MODELS) $\qquad$ IN. W.C. REFRIGERANT SUCTION $\qquad$ PSIG, SUCTION LINE TEMP* $\qquad$ REFRIGERANT DISCHARGE $\qquad$ PSIG, LIQUID TEMP $\dagger$ $\qquad$
() VERIFY REFRIGERANT CHARGE USING CHARGING CHARTS HIGH STAGE GAS HEAT TEMPERATURE RISE
RANGE (See Literature)
MEASURED TEMPERATURE RISE (HIGH STAGE)
LOW STAGE GAS HEAT TEMPERATURE RISE RANGE (208/230 VAC MODELS) $\qquad$
MEASURED LOW STAGE TEMPERATURE RISE RANGE (208/230 VAC MODELS)

* Measured at suction inlet to compressor
$\dagger$ Measured at liquid line leaving condenser.


[^0]:    * Part Numbers CPRCURB010A00 and CPRCURB011A00 can be used on both small and large basepan units. The cross supports must be located based on whether the unit is a small basepan or a large basepan. NOTES:

    1. Roof curb must be set up for unit being installed.
    2. Seal strip must be applied, as required, to unit being installed.
    3. Roof curb is made of 16 -gauge steel.
    4. Attach ductwork to curb (flanges of duct rest on curb).
    5. Insulated panels: 1-in. ( 25.4 mm ) thick fiberglass 1 lb . density.
[^1]:    Notes:
    ${ }^{1}$ Factory-shipped low stage cooling speed ${ }^{3}$ Factory-shipped low stage gas heating speed ${ }^{4}$ Factory-shipped high stage gas heating speed

[^2]:    "NA" = Not allowed for particular heating speed

[^3]:    1 Factory-shipped low stage cooling speed
    Factory-shipped low stage cooling speed
    2 Factory-shipped high stage cooling speed
    "NA" = Not allowed for particular heating speed

